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COMBATING HIGH-SULFUR FUEL

EFFECTS IN A TWO-CYCLE,
HIGH-SPEED U. S. ARMY DIESEL ENGINE

ADA 0 78798

INTERIM REPORT AFLRL No. 109



by

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Southwest Research Institute
San Antonio, Texas

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FOREWORD

The work reported herein was conducted at the U.S. Army Fuels and Lubricants Research Laboratory (USAFLRL), located at Southwest Research Institute, San Antonio, Texas under Contracts DAAG53-76-C-0003 and DAAK70-78-C-001. The contract monitor was Mr. F.W. Schaekel of USA-MERADCOM, and Mr. T. C. Bowen of the same office was project technical monitor.

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INTRODUCTION

A significant portion of the U.S. Army Combat/Tactical Fleet is powered by a single family of high output two-stroke cycle diesel engines. Table 1 gives a listing of vehicles using this engine family. The engine manufacturer recommends using diesel fuels with less than 0.5 wt% sulfur because "too high a sulfur content results in excessive cylinder wear due to acid build-up in the lubricating oil" (Ref-1). Previous investigations conducted by the United States Army Fuels and Lubricants Research Laboratory (USAFLRL) which used an aluminum block engine model 6V53T, revealed engine/fuel/lubricant incompatibilities when using fuels containing greater than 0.5 wt% sulfur and MIL-L-2104C (Ref-2) specification lubricants. The observed incompatibilities included catastrophic piston/ring/exhaust valve failure and relatively high deposit and wear rates (Ref-3). Additional documentation of the detrimental effects of high sulfur diesel fuel can be found in references 4 through 11.

Outside CONUS, the U.S. Army must at times use diesel fuels which contain up to 0.7 wt% sulfur as allowed by VV-F-800b, OCONUS (Ref-12) and even higher sulfur levels may be encountered in the future. Based on the fuel sulfur limit allowed OCONUS and the previous USAFLRL test results with two-cycle diesel engine and high sulfur fuel, a program was initiated to identify methods of counteracting the detrimental effects of high sulfur fuel. The program objective was to identify fuel and/or lubricant modifications which would allow continous operation on diesel fuel containing greater than 0.7 wt% sulfur without significantly reducing engine performance or service life. Identification of such fuel/lubricant modifications would expand the supply of diesel fuel available to the U.S. Army and potentially extend the service life of two-cycle diesel equipment. A previous report (Ref-13) covered the establishment of low and high sulfur fuel baselines using a constant lubricant in the iron block engine model 3-53. The current report covers the evaluation of various lubricants for their effectiveness in combating high sulfur fuel effects. Lubricant effectiveness was defined in terms of how well the lubricant performed as compared to the low and high sulfur fuel baselines.

TABLE 1. ARMY TACTICAL VEHICLES POWERED BY TWO-CYCLE DIESEL ENGINES

Designation	Description	Engine Model
M106A1	Mortar, Self-propelled. 107mm	6V53
M107	Gun, Self-propelled, 175mm	8V71T
M108	Howitzer. Self-propelled. 105mm	8V71T
M109	Howitzer. Medium. 155mm	8V71T
M110	Howitzer. Self-propelled	8V71T
M113A1	Carrier. Personnel	6V53
M125A1	Mortar. Self-propelled. Full-tracked	6V53
M132A1	Flame Thrower. Self-propelled	6V53
M548	Carrier. Cargo. Tracked. 3442 kg(6-ton)	6V53
M551	Armored Reconnaissance/Airborne	
	Assault Vehicle (Sheridan)	6V53T
M561	Gamma Goat	3-53
M557A1	Carrier. Command Post. Light Tracked	6V53
M578	Recovery Vehicle	8V71T
M746	Heavy Equipment Transporter (Het 70)	12V71T
XM667	Carrier. GM. Equipment. SP	a
XM727	Carrier. GM. Equipment. SP	a
XM730	Carrier. GM. Equipment. SP	a
XM741	Chassis, Gun, AA Artillery, 20mm, SP	a
XM806E1	Recovery Vehicle. FT Armored	a
	Truck, Dump, 18 140 kg (20-ton), Diesel Electric Driven	6V71

a = Vehicles are powered by either 6V53, 6V53T, or 8V71T (TB-750-652)

II. EVALUATION DETAILS

A. Test Engine

An iron-block, two-cycle diesel engine Model 3-53 was utilized as the test engine. This engine is the powerplant used in the M561 1-1/4T tactical truck (Gamma Goat). Additionally, this engine was used to minimize test fuel and engine rebuild costs per test while utilizing a "real-world" engine. Table 2 gives the characteristics of the 3-53 engine. The engine was fully instrumented and coupled to a laboratory test stand dynamometer. Figure 1 shows the test cell installation.

B. Test Technique

All tests were conducted using the U.S. Army 210-hour wheeled-vehicle test cycle (Ref-14) which has been correlated to 32,200 km (20,000 miles) of proving ground operation. This test cycle includes alternating periods of full-power and cold idling with an overnight shutdown as shown in Table 3. A complete description of the detailed procedure is presented in Appendix A.

C. Approach

As reported in the literature (Ref 4-11), increasing diesel fuel sulfur content causes increased engine wear and deposition. These effects were quantified in the 3-53 engine by establishing a low sulfur fuel baseline and a high sulfur fuel baseline while using a constant lubricant The low sulfur fuel baseline will serve as an example of desired performance level. The overall program objective is to identify fuel and/or lubricant modifications which will result in engine condition similar to the low sulfur baseline, when high sulfur fuel is used continuously. The low sulfur baseline was established using lubricant REO 203 and reference diesel fuel (0.4 wt% S) which is defined by Federal Test Method Standard 791B, Method 341.4. This combination had previously produced excellent results in the 6V53T engine (Ref-3). The high sulfur fuel (HSF) baseline was established using diesel fuel con-REO 203. taining 1.0 weight percent sulfur and lubricant

TABLE 2. 3-53 ENGINE CHARACTERISTICS

Engine type	Normally Aspirated, Two-cycle compression ignition, direct injection, uniflow scavenging
Weight (dry), kg (1b)	431 (950)
No. of cylinders, arrangement	3 in line
Displacement, liter (cu in.)	2.6 (159)
Bore and stroke, cm(in.)	9.84 x 11.43 (3-7/8 x 4-1/2)
Cylinder block material	cast iron (cast iron liners)
Rated power, kW(Hp)	72.3 (97) at 2800 rpm
Maximum torque, Nm(lb-ft)	278 (205) at 1800 rpm
Compression ratio	21 to 1
Fuel system	Unit injector (N 50 needle valve), primary and secondary engine filters)
Governor	Variable speed with throttle controls
Oil filter	Full-flow single filter
Oil cooling	Integral heat exchanger using 100 percent jacket-coolant flow capacity - 13.2 1 (14 qts)
Piston description Material/design Ring configuration	Cast iron/trunk type 1 - Fire ring (rectangular) 3 - Compression rings (rectangular) 2 - Oil rings

From jet in top of connecting rod

Piston cooling

FIGURE - 1

3-53 TEST CELL INSTALLATION

Diesel Engine Model 3-53 Test Facility (Full Power Fuel Cons. = 6.3 GPH)

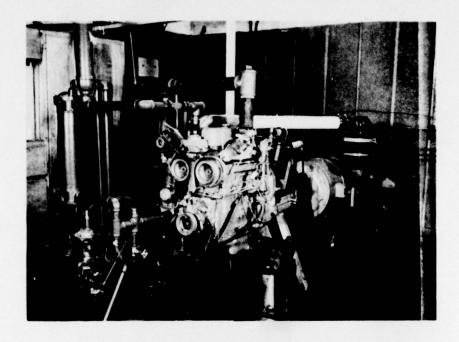


TABLE 3. WHEELED VEHICLE TEST CYCLE/DAY FOR 15 DAYS

Period	Time, hrs	Load, %	RPM	Coolant Temp, °C(°F)
1	2	100	2800	96 (205)
2	1	0	650	38 (100)
3	2	100	2800	96 (205)
4	1	0	650	38 (100)
5	2	100	2800	96 (205)
6	1	0	650	38(100)
7	2	100	2800	96 (205)
8	1	0	650	38 (100)
9	2	100	2800	96 (205)
10	10		Shutdow	n
	24			

Complete test is 15 days at 14 hr/day for 210 hours.

Industry was solicated for their help in developing potential solutions to the problem of continuous use of HSF. A letter (Appendix B) was sent to some 29 oil, chemical, and additive companies which requested that they submit fuel additives, lubricant additives, and/or completely formulated lubricants for evaluation. The request was also made during an SAE Open Forum on lubricants in Tulsa, OK during 1977. Materials for evaluation were received from five companies.

D. Test Details

All tests were conducted in 3-53 engine number 3D131703. Between tests new cylinder kits and clean exhaust valves were installed. Before test, the engine was measured for 1) liner bore (top/middle/bottom) at thrust/antithrust and front/back positions, 2) piston diameter, and 3) piston ring gap. After experiencing a blower drive gear failure in Test Number 3, the blower drive gears were replaced after each test. Pre- and post-test full load performance tests were determined using the test fuel.

The engine was operated in accordance with the procedure detailed in Appendix A and summarized in Table 3. The following hourly readings and calculations were made to monitor test operation:

Engine Speed
Engine Load
Torque
Observed Power
Fuel Rate
BMEP
BSFC

Temperatures

Jacket Coolant-In Jacket Coolant-Out Oil Sump Inlet Air (Blower) Exhaust Manifold Fuel at Filter

Pressures

Oil Gallery Blower Discharge Intake Vacuum Exhaust, Common Crankcase Averages of these readings and calculations are presented in the Appendix for each test.

After each test, the engine was disassembled and the following determinations were made:

- A. Engine condition ratings in accordance with standard CRC methods (Ref-15, 16) for:
 - 1. Ring face burning
 - 2. Ring sticking
 - 3. Liner scuffing and glazing
 - 4. Intake port deposits
 - 5. Ring deposits
 - 6. Piston deposits
 - 7. Exhaust valve condition
- B. Engine wear measurements for:
 - 1. Cylinder liner I.D. (top/middle/bottom)
 - 2. Ring gap
 - 3. Piston diameter

Oil consumption was calculated and photographs were made of significant engine parts. Used oils were analyzed to determine chemical and physical property changes. The above items are all included in the Appendix for each test.

III. SUMMARIZED RESULTS

This section will present summarized information about the lubricants evaluated, the test fuel used and overall test results. The following section will discuss each test in detail. Table 4 contains a summary of the 3-53 engine tests relevant to this report. The missing test numbers are for tests which were 1) reported earlier, 2) yet to be reported, or 3) not directly applicable. Test Number 1 is the low sulfur fuel (LSF) baseline, which is representative of the desired engine condition at end of test. The average of Test Numbers 4, 12, and 18 is the high sulfur

TABLE 4. SUMMARY OF 3-53 ENGINE TESTS

Test	Fuel		Lubricant	
No.	Sulfur, wt%	Code	Performance Level	Comments
1	0.4	REO 203	MIL-L-2104C	Low Sulfur fuel baseline
4	1.0	REO 203	MIL-L-2104C	High Sulfur fuel baseline
5	1.0	AL-6576	MIL-L-9000G	Navy 011
6	1.0	AL-6856	MIL-L-2104C	Army Reference Oil
11	1.0	AL-6942	MIL-L-2104C	Experimental Synthetic Oil
12	1.0	REO 203	MIL-L-2104C	High Sulfur fuel baseline
13	1.0	AL-7135	API SE/CD	Experimental Synthetic Oil
14	1.0	AL-7287	MIL-L-2104C/	
			MIL-L-46152	Mineral Oil
16	1.0	AL-6950	UK TS1033A	U.K. Reference Oil (ER-5)
18	1.0	REO 203	MIL-L-2104C	High Sulfur fuel baseline

fuel (HSF) baseline. Test Numbers 5, 6, 11, 13, 14, and 16 were evaluations of various lubricants for their effectiveness in combating high sulfur fuel effects. This effectiveness will be determined by comparing the after test engine conditions of a subject lubricant to the LSF and HSF baseline engine conditions.

During the time frame of these tasks, several batches of high sulfur diesel fuel (1.0 weight percent sulfur) were obtained from the same supplier. The fuel contained all straight run material. About 85% of the sulfur content was naturally occurring with the balance obtained through the addition of ditertiary butyl disulfide. All natural occurring sulfur in the test fuel was from the same refinery stream. Table 5 contains the analyses for the reference DF-2 (Test Number 1) and the high sulfur fuels used in this program.

The properties of the lubricants evaluated during this program are presented in Table 6. The low and high sulfur fuel baselines utilized a standard CRC reference engine oil (REO 203) which met the requirements and was qualified under specification MIL-L-2104C. The lubricant from Test Number 6 also met MIL-L-2104C requirements, and is considered a reference oil by the U.S. Army. Test Number 5 was run using a lubricant which met U.S. Navy specification MIL-L-9000G (SHIPS) (Ref-17). Test Numbers 11 and 13 evaluated synthetic based lubricants which were submitted by industry, and were approximately of MIL-L-2104C quality level. The oil evaluated in Test Number 14 was a mineral oil based product submitted by industry and had met the requirements of MIL-L-2104C. Test Number 16 used a mineral based lubricant which is designated a reference oil in the United Kingdom (U.K. ER-5).

Table 7 contains key average operating conditions for these tests. Included are parameters for power, fuel usage, operating temperatures and oil consumption. Table 8 contains a listing of test results including wear measurements for fire ring gap and liner bore change, piston and liner deposition ratings and other pertinent ratings. Table 9 shows a tabulation of the ring sticking performance for each test. Finally, Table 10 contains the used oil analyses which include the

TABLE 5. TEST FUEL PROPERTIES

				Test	No.		
Property	ASTM	1	4,5	6	11,12,13	14,16	18
Code	Method	Ref DF-2	AL-6765	AL-6933	AL-7178	AL-7289	AL-7766
API°	D 287	33.2	34.6	35.6	34.5	34.7	34.4
Sulfur, wt%	D 2622	ND	1.03	1.05	1.05	1.02	1.03
Sulfur wt%	D 1266	0.42	0.97	1.04	1.01	1.02	1.05
Viscosity, cS							
at 38°C	D 445	3.20	3.15	3.26	2.68 ^a	ND	2.81 ^a
Flash Point, °C	D 93	85	ND	54	73	79	82
Cloud Point, °C	D 2500	- 5	ND	ND	ND	ND	-15
Pour Point, °C	D 97	-8	ND	ND	ND	ND	-15
Water & Sediment	D 1796	0.0	0.0	0.0	ND	0.0	ND
Carbon Residue, wt%	D 524	0.10	0.19	0.17	0.18	0.19	ND
Copper Corrosion	D 130	1A	1B	1 A	1A	1A	ND
Cetane No.	D 613	47	ND	ND	ND	ND	48
Ash, wt%	D 482	0.006	0.001	0.001	ND	ND	ND
H. Htg Value,							
MJ/kg	D 240	45.47	44.82	44.60	45.00	45.00	ND
BTU/1b		19,500	19,300	19,200	19,400	19,400	
Distillation, °C	D 86						
IBP ·		210	197	186	197	204	200
10%		242	236	236	225	229	238
50%		271	274	272	262	263	269
90%		317	315	323	310	310	306
EP		365	349	365	352	363	344

ND = Not Determined a = Kvis @ 40°C

TABLE 6. TEST LUBRICANT PROPERTIES

					Test No.			
Property		1,4,12,18	5	9	11	13	14	16
Code		REO 203	AL-6576	AL-6856	AL-6942	AL-7135	AL-7287	AL-6950
K. Vis, cSt at 38°C		121.6	132.7	121.0	ND	UD	ND	ND
0.07		104.6	NO ON	ON	61.3	67.5	103,3	59.7
0,66		12.6	13.1	12.0	N	ND	ND	ON
100℃		11.8	ON ON	N ON	10.2	10.0	11.4	11.0
Viscosity Index		101	100	101	153	143	96	178
TAN		3.6	1.1	2.3	3.7	2.5	2.2	2.0
TBN		5.4	15.1	13.9	10.2	7.9	13.7	8.4
Insolubles, wt%								
Pentane A		0.05	0.02	0.04	60.0	0.03	NO	ND
Benzene A		0.04	0.01	0.04	0.01	0.01	ON ON	ND
Pentane B		0.03	0.02	0.03	0.09	0.01	ND	ND
Benzene B		0.02	0.02	0.01	0.02	0.01	ND ON	N O
API Gravity, °		27.5	25.9	25.5	21.9	18.4	25.5	29.1
Pour Point, °C		-21	-15	-17	41	-34	-21	-30
Flash Point, °C		241	241	223	227	227	227	226
Carbon Residue		1,19	1.63	2.10	1.53	1.12	1.82	0.56
Sulfated Ash, wt%	D 874	0.93	1.78	1.64	1.50	1.02	1,63	0.73
Elemental, wt%								
Ba		NIL	NIL	NIL	NIL	NIL	NIL	0.04
Ça	~	0.24	67.0	0.44	0.38	(60.0)	0.40	0.20
Mg		NIL	NIL	NIL	NIL	0.08	NIL	NIL
Zn Zn		60.0	0.05	0.07	0.18	0.13	0.14	60.0
А		60.0	0.08	0.08	0.12	0.11	0.11	0.05

ND = Not determined. XRF = X-ray fluorescence

TABLE 7. AVERAGE TEST OPERATING CONDITIONS

				Test No.				
Parameter	1 (LSF)	4,12,18(HSF)	5	9	11	13	14	16
Power (observed), kW	11	72	69.5	72	69.5 72 67	70	70	9/
Torque, nm	241	248	237	245	229	237	239	260
BMEP, kPa	586		572	593	552	572	579	627
Fuel Rate, kg/hr	9.61		18.3	20.02	18.0	18.4	18.3	20.0
BSFC, kg/kW-hr	0.276	0.264	0.275	0.278	0.268	0.264	0.262	0.262
Oil Temperature, °C	110		121	121	118	117	120	118
Exhaust Temperature, °C	207		497	518	493	502	508	547
Total Oil Consumption, kg	15.9		20.02	18.2	28.2	18.6	27.7	24.5

TABLE 8. TEST RESULTS Wear, Deposits, and Other Ratings

			T	Test No.				1
	LSF 1	HSF 4, 12, 18	2	9	11	13	14	16
Average Fire Ring Gap Change,	51	237	9/	330	203	Ą	102	279
Average Cylinder Liner Bore Change, Front-Back and Thrust-Antithrust, p Thrust-Antithrust only, pm	& & E I	16 23	10	20	23	8 15	15 20	20 25
Average Liner Scuffing, % Average Liner Glazing, %	4 5	41	31	33	26	28	22.	32
Deposition Piston WTD* Rating Cylinder 1 Cylinder 2 Cylinder 3 Average	226 318 356 300	393 374 345 371	391 440 487 439	452 494 426 457	446 370 363 393	534 488 407 476	367 341 401 370	336 461 531 443
Average Port Restriction, % Average Liner Lacquer, %	40	1 91	2 92	97	41 98	7 %	2 93	10 87
Other Average Ring Face Burning, % (Fire Ring + 1-3 Compression Rings)	1	32	32	87	31	=	28	42
Used Oil Iron Content, ppm at 210 hrs by XRF	110	117	8	8	09	95	82	149
The state of the s								

*WTD = Weighted Total Deposit A = Not determined, rings stuck

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TABLE 9. RING STICKING SUMMARY

Test No.	Ring Sticking (Cylinder-Ring-Condition)
1(LSF)	#2 - F/R - Sluggish #3 - F/R - 15% Cold Stuck
4 (HSF)	#3 - F/R - Sluggish
12(HSF)	#2 - F/R - 60% Cold Stuck
18(HSF)	#1 - CR#2 - 5% Cold Stuck
5	#1 - F/R - 10% Cold Stuck
6	#1 - F/R - Sluggish #2 - F/R - 30% Cold Stuck #3 - F/R - Sluggish
11	#1 - F/R - Sluggish #3 - F/R - 80% Cold Stuck
13	#1 - F/R - 90% Hot Stuck; #1 - CR#1 - Sluggish #2 - F/R - 100% Hot Stuck; #3 - CR#1 - Sluggish #3 - F/R - 100% Hot Stuck
14	#2 - F/R - 30% Cold Stuck
16	#1 - F/R - 10% Cold Stuck

Property	Method	LSF Baseline	Avg HSF Baseline	Test 5	Test 6	Test 11	Test 13	Test 14	Test 16
K. Viscosity at 100°C, cSt at 210 hrs \$\Delta\$ from new	D 445	119.8 ^a -1.8	123.2	158.3 ^a +25.6	173.5 ^a +52.5	75.3	71.0	136.6	60.1
<pre>K. Viscosity at 40°C, cSt at 210hrs Δ from new</pre>	D 445	12.9 ^b +0.3	13.4	14.9 ^b +1.8	15.5 ^b +3.5	11.8	10.5	13.9	10.0
TAN at 210 hrs	D 664	3.5	3.6	1.5	3.8	4.7	3.6	4.4	2.8
TBN at 210 hrs △ from new	D 2896	4.4	3.6	15.1	12.1	9.2	4.6	12.3	4.2
Flash Point, °C at 210 hrs \$\Delta\$ from new	D 97	238	252 +11	246	221 -2	232	260	241	232
Carbon Residue, wt% at 210 hrs △ from new	D 524	1.77	2.07	2.95	3.79	2.14	1.82	2.91	1.74
Sulfated Ash, wt% at 210 hrs △ from new	D 874	1.09	1.19	2.19	2.03	1.69	1.06	2.13	1.00
Insolubles, wt% (with coagulent) Pentane, at 210 hrs \$\Delta\$ from new	D 893	0.41	0.40	90.0+	0.83	0.03	0.03	0.08 ND	0.05 ND
Benzene, at 210 hrs Δ from new		0.28 +0.26	0.12 +0.10	0.07	0.73	0.02	0.23	0.07 ND	0.10 ND
Elemental, ppm at 210 hrs Fe Cr Cu Pb	AA (XRF)	(110) ND (< 50) 2	82 (117) 5 9 43	(90) < 5 (< 50) 8	(90) 8 7 16	61 (60) < 5 5 11	87 (95) < 5 < 1 16	82 (85) 5 6 8	114 (149) 11 9 11

a = Viscosity determined at 210°F b = Viscosity determined at 100°F ND = Not determined values of selected properties determined at the end of test (210-hours) and the change in property value from new. Having presented the overall summary of test operation and results, each individual test will be discussed in the following section.

IV. DISCUSSION OF RESULTS

In this section, each test will be discussed based on the data presented in Tables 6 through 10. Each test lubricant will be compared to the low and high sulfur fuel baselines to provide an overall assessment of lubricant performance in combating high sulfur fuel effects.

Before discussing the individual tests, the key performance areas of the low and high sulfur fuel baselines will be reviewed. The results of the LSF baseline (Table 8) are representative of the desired engine condition of the test. Measured wear (fire ring gap and cylinder liner bore) were low as were liner scuffing and ring face burning. Piston deposit levels were moderate, and no serious ring sticking problems were observed. Compared to the LSF baseline, the HSF baseline had much more severe ring face burning (32% vs 1%) and cylinder liner scuffing (41% vs 4%). Measured wear was two to four times more severe for the HSF baseline. Piston cleanliness had deteriorated slightly and ring sticking tendency had increased slightly, but still did not approach problem levels. As shown in Table 10, the used oil from the LSF test was still in satisfactory condition while the HSF lubricant had been degraded only slightly more (mainly an increase in flash point and a slight increase in viscosity). The HSF baseline lubricant had increased to SAE 40 viscosity after test, but this was not severe as the new oil itself was on the borderline of being SAE 40. In evaluating the performance of the various test lubricants in combating HSF, our primary objective was to obtain engine condition approaching or equal to the LSF baseline condition when the engine was operated using HSF.

Test Number 5

The lubricant (AL-6576) evaluated in Test Number 5 met the requirements and was qualified under specification MIL-L-9000G (SHIPS) and was viscosity grade SAE 40. It contained a calcium based detergent-dispersant additive system and had a rather high sulfated ash content (1.78 weight percent), and high total base number (15.1).

This test resulted in some improvement in overall engine condition as compared to the HSF baseline. As shown in Table 8, fire ring gap wear was significantly reduced while liner bore change and liner scuffing were slightly reduced with AL-6576. No improvement in ring face burning was observed and a detriment in piston cleanliness resulted. No significant ring sticking occurred during this test (Table 9). Used oil analyses (Table 10) revealed that the condition of AL-6576 was not significantly degraded. While Test Number 5 showed some marked improvement over the HSF baseline, its overall performance did not approach the excellent performance observed for the LSF baseline, except for fire ring end-gap wear which were comparable.

Test Number 6

The lubricant (AL-6856) evaluated in Test Number 6 met the requirements and was qualified under specification MIL-L-2104C, SAE grade 30, and is considered by the Army to be a MIL-L-2104C reference lubricant. This oil contained a calcium based detergent-dispersant additive system with a sulfated ash of 1.64 weight percent and a total base number of 13.9.

As shown in Table 8, use of this lubricant resulted in no significant improvement in engine condition as compared to the HSF baseline. In fact, fire ring gap wear was much more severe as was ring face burning. Piston deposit levels were consistently higher than the HSF baseline. Only the average cylinder liner scuffing showed a slight improvment in Test Number 6. Ring sticking (Table 9) was similar to that observed in the HSF baseline tests. The used oil analyses (Table 10) revealed that AL-6856 thickened from an SAE 30 to an SAE 40 viscosity grade during the

test. This increase was probably caused primarily by soot accumulation as the carbon residue and insolubles values increased significantly during the test. Overall, the use of AL-6856 did not reduce or counteract the detrimental effects of using HSF.

Test Number 11

The lubricant (AL-6942) evaluated in Test Number 11 was described by its manufacturer as "an experimental synthetic non VI-improved SAE 10W-30 lubricant." Discussions with the manufacturer revealed that AL-6942 was a blend of synthesized hydrocarbon and ester material. AL-6942 was formulated to meet the requirements of MIL-L-2104C and API service classification SE. This oil contained a calcium based detergent-dispersant additive system, with a sulfated ash of 1.50 weight percent and a total base number of 10.2.

Compared to the HSF baseline, Test Number 11 had very similar results as shown in Table 8. The average cylinder liner scuffing was slightly reduced for Test 10. However, the key areas of ring face burning and measured ring and liner wear were not significantly improved. Piston cleanliness (Table 8) and ring sticking (Table 9) were comparable to the HSF baseline. The used oil properties (Table 10) indicated that the lubricant was still in satisfactory condition at 210 hours as there were no substantial changes in oil properties. Overall, the use of AL-6942 did not result in the desired engine condition when high sulfur fuel was used.

Test Number 13

The lubricant (AL-7135) evaluated in Test Number 13 was described by its manufacturer as a "polyol ester based lubricant which contains no viscosity index improver." AL-7135 was formulated to meet the requirements of API service classifications SE and CD. The oil contained a mixed calcium and magnesium based detergent-dispersant additive system which resulted in a sulfated ash of 1.02 weight percent and a total base number of 7.9.

As shown in Table 8, evaluation of AL-7135 resulted in very good performance in some areas and very bad performance in other areas. Relative to the HSF baseline, Test 13 showed good improvement in overall average cylinder liner bore wear, and a very significant reduction in ring face burning, while the average cylinder liner scuffing was moderately reduced. Unfortunately, the use of AL-7135 resulted in severely hot-stuck fire rings in all three cylinders (Table 9). Piston deposits were rather heavy which probably was a consequence of the stuck fire rings. The used oil analyses (Table 10) revealed a large increase in flash point of the lubricant (+33°C) and a significant reduction in total base number. Other lubricant properties were not significantly degraded. Overall, the use of AL-7135 offered promise for controlling some of the HSF effects such as ring face distress; however, the hot stuck fire rings negate the possible use of this lubricant as a solution to the HSF problem.

Test Number 14

The lubricant (AL-7287) evaluated in Test Number 14 was described by its manufacturer as a "mineral base stock oil that meets the performance requirements of MIL-L-46152 and MIL-L-2104C." The lubricant was viscosity grade SAE 30 and had a calcium based detergent-dispersant additive system. The sulfated ash was 1.63 weight percent and the total base number was 11.4.

Compared to the HSF baseline, the use of AL-7287 resulted in mixed performance (Table 8). Ring face burning was much more severe with AL-7287, while the average cylinder liner scuffing was moderately reduced. The average fire ring gap wear was significantly reduced in Test 14, while the cylinder liner bore wear, piston deposit ratings, and ring sticking (Table 9) were very similar to the HSF baseline. The used oil analyses (Table 10) show that the viscosity had increased to an SAE 40 grade and that the flash point had increased moderately (+14°C). The carbon residue had increased (+1.09 weight percent) indicating a buildup of combustion byproducts, while the insolubles did not reach significant levels.

Overall, AL-7287 did not approach the desired level of performance observed in the LSF baseline.

Test Number 16

The lubricant (AL-6950) evaluated in Test Number 16 was a United Kingdom reference oil (ER-5). AL-6950 was evaluated because it had given acceptable performance in a United Kingdom four-cycle diesel engine test which used high sulfur fuel (1.0 weight percent). This lubricant contained conventional petroleum basestocks and met the viscosity requirements of SAE 10W-30. AL-6950 had a calcium based detergent-dispersant additive system with a sulfated ash of 0.73 weight percent and a total base number of 4.8.

Compared to the HSF baseline, the use of AL-6950 did not result in any significant improvement in engine condition (Table 8). Measured wear (fire ring gap and cylinder liner bore), ring face burning and piston deposits were all equal to or worse than the HSF baseline. No serious ring sticking was encountered with AL-6950 and the used oil analyses (Table 11) showed only a moderate increase in flash point (+7°C). The used oil iron content was slightly higher than the HSF baseline. Overall, the use of AL-6950 did not result in the desired level of performance observed in the LSF baseline.

V. CONCLUSIONS/RECOMMENDATIONS

A qualitative summary assessment of the performance of the lubricants tested in this program is presented in Table 11. The following conclusions are made based on the work covered in this report:

- To date, none of the lubricants tested would allow the continous use of HSF without a penalty in engine condition as compared to LSF utilizaton.
- o One lubricant (AL-6576) which met the requirements of specification MIL-L-9000G (SHIPS) yielded significant improvement in measured wear, but no improvement in ring face condition when high sulfur fuel was used.

TABLE 11. SUMMARY OF LUBRICANT PERFORMANCE COMPARED TO HSF BASELINE

Test No.						
5	6	11	13	14	16	
AL-6576	AL-6856	AL-6942	AL-7135	AL-7287	AL-6950	
++		0	A	+		
o		o	++			
+			++	0		
+	+	+	+	+	+	
		0		0		
o	o	o		o	0	
	++ 0 + +	++ 0 + + +	5 6 11 AL-6576 AL-6856 AL-6942 ++ 0 0 0 + + + + + 0	5 6 11 13 AL-6576 AL-6856 AL-6942 AL-7135 ++ 0 A 0 0 ++ + ++ + + + + 0	5 6 11 13 14 AL-6576 AL-6856 AL-6942 AL-7135 AL-7287 ++ 0 A + 0 0 ++ + + + + + + + + + + + + + + 0 0	

^{++ =} Improvement approaching LSF baseline

^{+ =} Improvement

^{-- =} Worse than HSF baseline

o = Approximately the same

A = Not determined, rings stuck

- Lubricant AL-7135 gave improved performance in measured wear and ring face condition compared to the HSF baseline; however, severe fire ring sticking occurred with this oil which precludes further evaluations of it.
- The other lubricants tested with HSF resulted in slight or no overall improvement in engine condition. (Some even resulted in worse performance than the HSF baseline).

The following recommendations for future effort are offered:

- Additional lubricants which are specially formulated to counteract the deleterious effects of using HSF should be developed and tested.
- Additional lubricants from within the military supply system should be tested with HSF (e.g. MIL-L-21260B Preservative Oil, and MIL-L-46167 Arctic Engine Oil) to further define the current status of the problem.
- Fuel additives for combating HSF effects need to be identified and tested.
- Additional effort needs to be undertaken to aid in the base understanding of the fuel combustion and engine degradation mechanisms involved with HSF.
- Future Army engine oil specifications should include both two and four cycle diesel engine test requirements using HSF.

VI. ACKNOWLEDGEMENTS

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Mr. J.W. Pryor Technical Editor

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Mr. Jesse Cantu Drafting

Ms. R.J. Shew Typing

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APPENDIX A

Wheeled-Vehicle Test Procedure

APPENDIX

WHEELED-VEHICLE TEST PROCEDURE DD 3-53 ENGINE

Test	No.:	Engine Serial No.:	Test Cell No.: _
Test	Lubricant:	Test Fuel:	

Instructions

- 1. Pre-Test Preparations.
- 1.1 Filter Elements. Install new element in oil filter and change oil in air filter bath (using test oil).
- 1.2 Sump Oil Charge. Charge engine sump to full mark on dipstick with test oil (AL- -L). Close filler cap and motor engine for one minute at low speed (about 500 RPM) to fill oil cooler, filter, and internal oil passages. Recheck level and add to full mark again (should be about 25 lbs).
- Priming Fuel System. After changing over to Ref DF-2 fuel and flushing fuel lines, remove the Allen plug from top of primary fuel filter and fill the filter with fuel, then re-install plug.
- Break-In Procedure. Set jacket coolant-out temp. controller at 205°F. Start engine and idle at 650 RPM for five minutes, then warm up at about 1000 to 1200 RPM for ten minutes. If no engine malfunctions or leakages occur, conduct the following break-in and record complete log sheet readings at end of each setting. Calculate: BHP, Torque, BSFC, BMEP.

Time Minutes	Speed RPM	Load 1b	Jacket-Out Temperature
30	1800	25	205
30 30	2200	55	205
30	2500	80	205
30	2800	80	205



1.5 Full Load Performance Test. Following the break-in run, conduct a full load performance test run at the following conditions. Allow conditions to stabilize at each speed, then record complete log sheet readings at end of each setting. Calculate BHP, Torque, BSFC, BMEP.

Speed, RPM	Jacket-Out, °F
1600	205
1800	205
2000	205
2200	205
2400	205
2600	205
2800	205

- 1.6 Valve Clearance Check. Upon completing the full load performance test, stop engine and immediately check the hot clearance of the exhaust valves. Adjust clearances to .023-.025 in, also check injector height per gauge.
- 1.7 Oil and Fuel Change-Over. Upon completing valve clearance check, drain oil sump and filter. Discard drain and oil filter element. Weigh and record (on oil consumption log) a new oil filter element. Install new oil filter and then charge system with full charge of test oil (AL--L) as in item 1.2. Record weight of total charge. Change over to test fuel (AL--F) and flush fuel lines. Replace both fuel filter elements and prime as in item 1.3. Weigh oil blowby can and record (oil consumption log).
- $\frac{\text{Full Load Performance Test.}}{\text{full load performance test}}. \quad \text{Following fuel change-over, run}$

Check and Adjust Oil Level Before Starting Test.

- 2. Test.
- 2.1 Warm-Up. At the start of each day--idle for five minutes, then start test cycle at 2800 RPM.
- 2.2 <u>Test Conditions</u>. After warm-up, the following test cycle conditions are followed:

Test Cycle for 15 Days

Period	Time, Hrs	Load, %	RPM	Coolant Temp., °F
1	2	100	2800+20	205+2
2	1	0	650+25	100+2
3	2	100	2800	200
4	1	0	650	100
5	2	100	2800	205
6	1	0	650	100
7	2	100	2800	205
8	1	0	650	100
9	2	100	2800	205
10	10		-Shut Down	

Operate at test conditions 14 hours/day for a total of 210 hours. Complete log sheet readings at end of each period. Calculate: BHP, Torque, BSFC, BMEP.

- 2.3 Daily Cool-Down. After the last test hour each day, reduce the speed to idle (600-650 RPM) for five minutes, (without resetting coolant controller) then stop engine.
- 2.4 <u>Used Oil Samples</u>. Flush oil filter tap, and withdraw a used oil sample during daily 5-minute cool-down (item 2.3) according to the Oil Consumption Log schedule and record sample weight.

Identify each sample as to test hours, test No. and oil code (AL- -L). Take: 2 oz. sample each day except at 70 and 140 hours take 12 oz. sample. At end of test take 16 oz. sample. Take daily oil samples to Chem Lab for elemental analyses by XRF.

- 2.5 Oil Additions. New test oil additions, if required, are to be made at the end of each day after shutdown. Allow five minutes for oil to drain back to sump. Add weighed new oil to restore sump level to full by dipstick. Record weight of add-on oil consumption log.
- 2.6 Final Oil Drain. Upon completion of post test power curves and while engine is warm, drain the sump, saving one gallon of used oil in clean can. Tag can, showing test No., oil code, date, and test hour. Also remove oil filter element, weigh and record.

2.7 Notes and Limits.

- (1) Coolant is 50% glycol/50% water.
- (2) Coolant Out temperature must be reduced to 100°F within 15 minutes after idle starts.
- (3) Limits/Tolerances: Coolant Out Temperature: +2°F of designated temperature.

Oil Sump Temperature: 265°F max.

Fuel @ Filter Temperature: 90+5°F (105°F max.=shutdown).

- (4) No Oil Change during test.
- After Test.
- 3.1 Full Load Performance Test. At end of test, run full load performance test as in item 1.5.
- 3.2 <u>Valve Clearance Check</u>. Upon completing end of test power curve, item 3.1, check hot valve clearances and record.
- 3.3 Wear and Deposits. Upon disassembly of engine, check wear measurements and deposit ratings (on sheets provided).
- 3.4 Record amount of fuel used for test.
- 3.5 Calculations (for AFLRL Cell No. 2: BHP (obs.) = $\frac{\text{Load x RPM}}{3000}$

Torque (1b-ft) = Load x 1.75 BSFC (1b/Bhp-hr) = 1bs Fue1 per hr/BHP (obs.) BMEP (psi) = Torque x 0.474

- 4. Cell Notebook.
- 4.1 Keep cell notebook updated (like a diary) at all times.
 Record what is being done (changes or repairs) to the cell
 engine, instruments, etc. Record anything unusual and all
 modifications.

OIL CONSUMPTION LOG

Oil Addition Record Oil Code Test No. Test Op. Weight Oil & Can | Weight Oil & Can | Weight of Wt Initial Hours Init. Before Add After Add Oil Added Oil Fill 14 28 Wt Total 42 Oil Adds 56 70 Wt Fill 84 Plus Adds 98 112 Wt Total 126 Oil Samples 140 154 Wt Final 168 Oil Drain 182 196 Wt Used 210 Filter Total Additions Wt New Filter

Oil Samples

Test	Op.	Weight of	
Hours	Init.	Sample & Bottle	Weight of Sample
14			
28			
42			
56			
*70			
84			
98			
112			
126			
*140			
154			
168			
182			
196			
*210			
		Total Samples	

Wt Oil in Filter

Total Oil Drains

Total Oil Cons.

All Weights are in Pounds.

* - Large Samples - 12 oz.; all others are 2 oz.

APPENDIX B

Letter to Oil, Chemical, and Additive Companies



DEPARTMENT OF THE ARMY Bowen/mb/43576 US ARMY MOBILITY EQUIPMENT RESEARCH & DEVELOPMENT COMMAND FORT BELVOIR, VIRGINIA 22060

DRDMEGL

14 July 1977

SEE DISTRIBUTION LIST

Gentlemen:

In our letter of 2 March 1977 concerning multigraded engine oil, we indicated the Army was experiencing a problem with high-sulfur diesel fuels. The purpose of this letter is to solicit your assistance in developing a solution to this problem. The difficulty occurs during the continuous operation of Army diesel powered equipment on high-sulfur fuel (>0.5%S). Diesel fuels purchased OCONUS by the Army are consistently running in excess of 0.5% sulfur and have contained as much as 1.2% sulfur. The problem is more critical in two-cycle diesel engines with engine failures reported from areas where high-sulfur fuels have been used. The Army fleet contains a significant number of two-cycle diesel powered engines as shown by Table 1. Laboratory investigations have confirmed the effect of high-sulfur diesel fuel on Army two-cycle diesel equipment (SAE paper No. 760717). Specific problem areas documented by the laboratory investigations included: catastrophic piston/ring/exhause valve failure and relatively high deposit and wear levels.

Fuel and/or lubricant modifications hold promise for solving the Army's problem of operating continuously on high-sulfur fuel. The Army envisions three possible approaches, which include:

Approach No. 1: a fuel additive added at the refinery which would counteract the deleterious effects of fuel sulfur combustion products. This additive would be requested for use only in areas where high sulfur diesel fuel is being used continuously.

Approach No. 2: a lubricant additive package added by the lubricant blender to current MIL-L-2104C qualified products. This package must be completely compatible with all qualified MIL-L-2104C products and must allow continuous operation on high-sulfur fuels while still maintaining excellent overall MIL-L-2104C performance. This lubricant would be used only where continuous operation on high-sulfur fuels is encountered.



Approach No. 3: a new generation of diesel lubricants containing a specially balanced and formulated additive package to give excellent performance in both two and four-cycle diesel engines operated on high-sulfur fuel. In addition to meeting future anticipated MIL-L-2104C requirements as defined in our letter of 2 March 1977, this new generation of lubricants would directly replace the current MIL-L-2104C lubricant for use in all nonarctic operated Army combat/tactical equipment.

If Approach No. 3 is taken, the Army would like to ultimately see the new generation lubricant include multigrade technology as discussed at the SAE open forum in Tulsa, Oklahoma (June, 1977). It is understandable and acceptable to the Army if lubricant/additive suppliers determine that multigrade technology and high-sulfur fuel/lubricant technology each must be developed separately and in a stepwise manner. However, the ultimate lubricant desired must have both multigrade characteristics and be able to counteract the deleterious effects of high-sulfur fuel.

Currently the Army is developing baseline information on fuel sulfur effects in the DDAD 3-53 engine which is the power plant in the Army's 1-1/4 ton M561 (Gamma Goat). The engine has been installed at the U.S. Army Fuels and Lubricants Research Laboratory in San Antonio, Texas. Once baseline determinations are completed, the exact performance target can be set. Presently, we are defining acceptable performance with high-sulfur fuel (1.0%S) as wear and deposition not greater than that obtained from a reference lubricant (REO 203) and low-sulfur fuel (0.4%S) in the 3-53 engine. The test procedure being followed is the Army's 210-hour wheeled-vehicle test cycles as defined in SAE paper No. 760717. If approaches 2 or 3 are followed, the Caterpillar OL-1 test will be used in addition to MIL-L-2104C requirements to determine four-cycle compatibility of the new lubricant. If approach No. 1 is followed, the fuel additive supplier must submit data showing both twocycle and four-cycle diesel engine compatibility for his proposed fuel additive.

Suppliers who believe they could furnish a product meeting the requirements described herein should forward a 50-gallon drum of the finished lubricant or sufficient fuel additive to treat 2000 gallons of fuel to:

U.S. Army Fuels and Lubricants Research Laboratory Southwest Research Institute Attn: Mr. E. A. Frame 8500 Culebra Road San Antonio, Texas 78284 Page 3

An additional 5-gallon finished lubricant sample or 1-gallon fuel additive sample should be sent to:

Commander

U.S. Army Mobility Equipment Research & Development Command Attn: DRDME-GL, Mr. T. C. Bowen Ft. Belvoir, Virginia 22060

Priority will be given to lubricant samples submitted with MIL-L-2104C engine test data and the Caterpillar OL-1 test results and to fuel additives with engine test data supporting the recommendation. The Army will conduct the previously mentioned 3-53 two-cycle diesel engine tests.

In closing, suppliers are again reminded that (1) the Army diesel-powered fleet has a special lubrication requirement; i.e., operation over any kind of terrain, under all kinds of climatic conditions coupled with the combined requirements of a diverse inventory of specialized ground-powered equipment and extremely severe operating cycles, (2) test results will be provided to suppliers; however, test data generated by the Army does not constitute an official endorsement of any lubricant or fuel additive.

Sincerely yours,

Maures & LoCene

Chief, Fuels & Lubricants Division

MAURICE E. LEPERA

1 Incl

CF: AFLRL

Table 1 Army Tactical Vehicles Powered by GMC Detroit Diesel Two-Cycle Engines

Designation	Description	Engine Model
M106A1	Mortar, Self-Propelled, 107 MM	6V53
M107	Gun, Self-Propelled, 175 MM	8V71T
M109	Howitzer, Self-Propelled, 105 MM	8V71T
M109	Howitzer, Medium, 155 MM	8V71T
M110	Howitzer, Self-Propelled	8V71T
M113A1	Carrier, Personnel	6V53
M125A1	Mortar, Self-Propelled, Full-Tracked	6V53
M132A1	Flame Thrower, Self-Propelled	6V53
M548	Carrier, Cargo, Tracked, 6-Ton	6V53
M551	Armored Reconnaissance/Airborne Assault Vehicle (Sheridan) 6V53T
M561	Gamma Goat	3-53
M577A1	Carrier, Command Post, Light Tracked	6V53
M578	Recovery Vehicle	8V71T
M116	Cargo Carrier, Amphibious, Tracked,	3-53
HET70	Heavy Equipment Transporter	12V71T
XM 667	Country CN Frankrich CR	
XM 727	Carrier, GM, Equipment, SP	*
XM 730	Carrier, GM, Equipment, SP	*
XM 741	Carrier, GM, Equipment, SP	*
	Chassis, Gun, AA Artillery, 20 MM, SP	*
XM 806E1	Recovery Vehicle, FT Armored	*
	Truck, Dump, 20-Ton, Diesel Electric Driven	6V71

*Vehicles are powered by either 6V53, 6V53T, or 8V71T (TB-750-652).

Note: All new and rebuilt series 53 engines use trunk-type pistons. Only the recently procurred and currently rebuilt series 71 engines use the cross-head type piston.

DISTRIBUTION LIST

Amoco Chemical Corporation (G. Barth) Amoco Oil Company (C. Sechrist) Atlantic Richfield Co. (Frank J. Chloupek) Bray Oil Company (M.Z. Fainman) Chevron Chemical Co. (W. Wagner) Chevron Research Co. (W. Long) Continental Oil Co. (W. Council) Edwin Cooper, Inc. (D. W. Dinsmore) E. I. DuPont de Nemours & Co. (P. Polss) Emery Industries (R. Boehringer) Ethyl Corp. (J. Kozikowski) Exxon Research & Engineering Co. (Walter Waddy) Gulf Oil Canada (J. E. McCormack) Gulf Oil Chemicals Co. (M. Campen) Imperial Oil Enterprises (G. Holmes) Lubrizol Corp. (J. Creedon) Mobil Research & Development Corp. (V. Lowther Paramins Laboratories (A. Schetelich) Petrolite Corp., Tretolite Div. (Grenzer) Phillips Petroleum Co. (K. Yochum) Rohn & Haas (R. Schum) R. T. Vanderbilt Company, Inc. (W. Suyden) Shell Research & Development Corp. (D. Olson) Standard Oil of Ohio (R. L. Pontious) Stauffer Chemical Co. (G. Berens) Sun Oil Co. (W. Crouse) Texaco Inc. (R. Paggi) Union Oil Co. (F. Liggett) W. R. Grace, Hatco Chemicals (J. Newcomb)

APPENDIX C

3-53 TEST #5

FUEL: 1% S, DF-2

LUBE: MIL-L-9000G, AL-6576

START: 30 MARCH 1977

END: 19 APRIL 1977



ENGINE OPERATING DATA (AVG) TEST #5

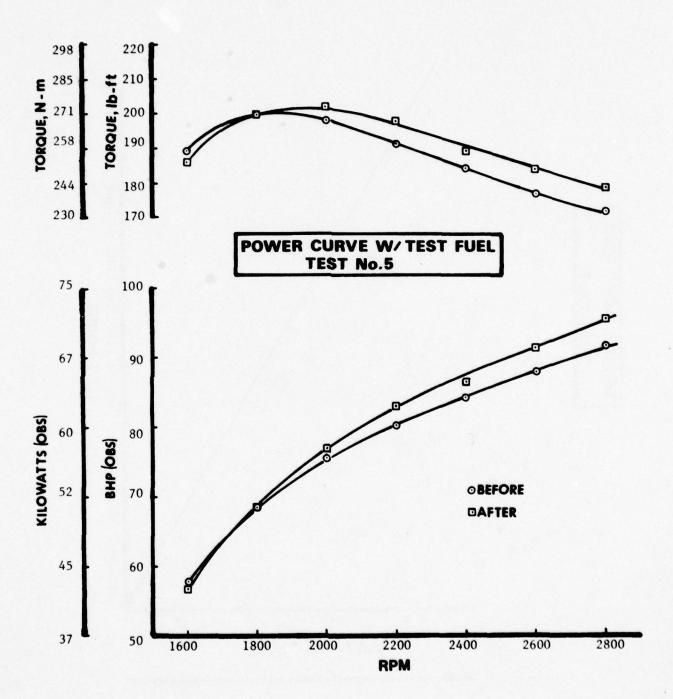
	Min	Power Max	Avg	Idle (Avg)
Engine Speed, rpm	2797	2808	2802	645
Load, 1bs	98	102	99	
Torque, 1b-ft	171.5	178.5	174.8	
BHp obs	91.5	95.2	93.2	
Fuel Rate, 1b/hr	39.5	43.7		
BMEP, psi	81.3	84.6		
BSFC 1b/BHp-hr	.429	.466	.452	
Temperatures, °F				
Jacket Coolant-In	194	199	196.5	94
Jacket Coolant-Out	204	205	204.3	100
Oil Sump	248	253	250.5	200
Inlet Air (Blower)	70	104	89.5	
Exhaust Manifold	810	950	926	
Fuel @ Return	139	150	144.7	
Pressures	133	130	111.1	
Oil Gallery, psig	42.0	45.6	43.5	29
Blower Discharge,	7.2	8.6	8.1	
Airbox, psig	7.2	0.0	0.1	
Intake Vacuum, in. H ₂ 0	6.4	7.4	7.0	
			3.0	
Exhaust, Common, in. Hg	2.7	3.3	3.0	



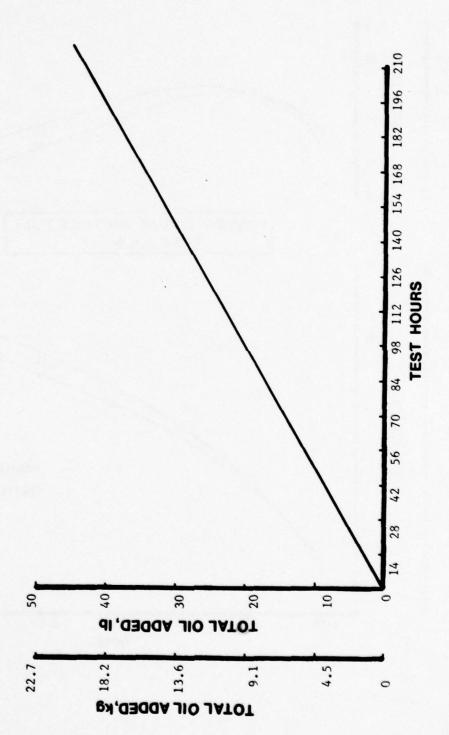
LUBRICANT ANALYSES (AL-6576) TEST #5

Property	ASTM Method	New Oil	70 Hrs	140 Hrs	210 Hrs
K. Vis, cS, 38°C (100°F) K. Vis, cS, 99°C (210°F) VI TAN TBN Insolubles, wt%	D445 D445 D2270 D664 D2896 D893	132.7 13.1 100 1.1 15.1	145.3 14.1 101 2.0 13.7	155.7 14.7 101 1.9 15.4	158.3 14.9 102 1.5 15.1
Pentane A Benzene A Pentane B Benzene B	D033	0.02 0.01 0.02 0.02			0.04 0.03 0.08 0.07
API Gravity, ° Pour Point, °C Flash Point, °C Carbon Residue, wt%	D287 D97 D92 D524	25.9 -15 241 1.63	2.40		24.6
Sulfated Ash, wt% Elemental Ba, ppm	D874 Method XRF	1.78 < 300	1.98	2.82 2.13	2.95 2.19
Mg, ppm Ca, wt% Zn, wt% Na, ppm	AA XRF/ <i>AA</i> XRF/ <i>AA</i> AA XRF	4 0.55/0.49 0.05/0.05			132
Cu, ppm Cr, ppm Pb, ppm Sn, ppm Fe, ppm C1, ppm	AA AA AA XRF XRF	 540	72	90	< 30 < 5 8 < 50 90

^{--- =} Not Determined.
AA = Atomic Absorption.
XRF = X-Ray Fluorescence.



NET OIL ADDITIONS TEST No.5



RING FACE CONDITION: % BURNING TEST #5

	Cylinder Number			
	1	2	3	
First Ring	3	90	15	
Second Ring	1	3	15	
Third Ring	N	70	80	
Fourth Ring	N	30	80	
Average of all	32%			
Average w/o Cyl-1	48%			
Average w/o cyl-1	100	•		

N = Normal

RING STICKING TEST #5

Ring	Piston Number				
Ring No.	1	2	3		
1	10% Cold Stuck	F	F		
2	F	F	F		
3	F	F	F		
4	F	F	F		

F = Free

CYLINDER LINERS TEST #5

		% Lacquer	85	92	95	92
		% Glazed	15	rv	Ŋ	∞
Cyl Perce	Area Scuffed	2.8	25	40	31	
	Anti-Thrust	20	45	7.5	5.7	
	Thrust	S	5	5	S	
	Restriction	2	2	М	2	
	Cylinder	Number	1	2	3	Average
	Percent of Compression Ring	Percent of Compressic Travel Area Percent Scuffed	fed % Glazed	Percent of Compression Ring Travel Area Restriction Thrust Anti-Thrust Area Scuffed 2 5 50 50 28 15	Percent of Compression Ring Percent Port Travel Area % Total Restriction Thrust Anti-Thrust Area Scuffed % Glazed 2 5 50 28 15 2 5 45 25 5	Percent of Compression Ring Percent Port Restriction Percent Scuffed & Total % Total 2 5 50 28 15 2 5 45 25 5 3 5 75 40 5

PISTON O.D. (IN) TEST #5

3	3.8710	3.8710	0
2	3.8710	3.8710	0
	3.8710	3.8710	0
Cylinder	Before	After	٧

	Piston Number			
	1	2	3	
Top Land	N	N	N	
Skirt	N	Lt. Scratch	Lt. Scratch	
Piston Pin	N	N	N	

PISTON GROOVE INSIDE DIAMETER - % RING SUPPORTING CARBON TEST #5

		P	iston Numbe	er
Piston Ring	Quadrant	1	2	3
	1	80	85	90
1	2	0	0	0
	3	0	0	15
	4	0	0	5
	1	0	40	5
2	2	15	0	100
	3	0	5	95
	4	0	100	0

Quadrants:

1 = Thrust 2 = Rear 3 = Anti-thrust 4 = Front

EXHAUST VALVE DEPOSITS TEST #5

	Cylinder No.
Area	1 2 3
Head	All 100%-AHC to Soot
Face	All 100%-9 to Clean
Tulip	A11 100%-9
Stem	All 50%-9 to Clean

EXHAUST VALVE SURFACE CONDITIONS TEST #5

		Cylinder No.	
	1	2	3
Freeness in Guide	F	F	F
Head		All Normal	
Face	Signs o	f Leaking	N
Seat	Leaking	OK	ОК
Stem		All Normal	
Tip		All Normal	

RING DEPOSITS TEST #5

Cylinder Number Ring	Number	CARB	LACQ	CARB 2	LACQ	CARB	LACQ
Top	1 2	90-1/2 AHC 0	10-8 95-9	10-1/2 AHC 0		10-1/2 AHC 10-1/2 AHC	95-9 90-9
	3	. 0	10-8	0	15-8, 55-/ 5-9	0	100-9
	4	0	100-3	0	95-8 100-5	0	100-2
10	1	100-1/2 AHC	0	15-AHC	0	100-1/2 AHC	0
	2	100-AHC	0	85-1/2 AHC 100-AHC	0		0
57	3	100-1/2 AHC	0	25-AHC	0		0
J. 7	4	100-1/2 AHC	0	/5-1/2 AHC 0	100-9	90-1/2 AHC 0	100-9
Bottom	1	0	20-7	0		0	100-3
	2	0	10-5	0	5-8, 10-7 100-3	0	5-9, 25-7
	3	0	40-3	0	50-3	0	80-3 100-4
	4	0	100-2	0	30-2 100-2	0	100-2

CRC DIESEL RATING SYSTEM

STANDARD COMPUTATION SHEET FOR PISTON RATING RATER E.R. Lyons DATE 4-25-77

PISTON NO1	NO. 1 GROOVE, VOLUME-%	PISTON WTD . RATING
RATER E.R. Lyons DATE 4-25-77 LABORATORY TEST NUMBER 3-53-5 STAND NO. 2 ENGINE NO. 3D-131703	FUEL 1% S, DF-2	
TEST PROCEDURE TEST HOURS 210 TEST LABORATORY AFLRL	LUBRICANT AL-6576	

															-	
	-				GRO	GROOVES						LANDS	S		UNDER	
DEPOSIT	SIT DEPOSIT	Z	NO. 1	2	NO. 2	Ž	NO. 3	NO. 4	NO. 1		NO. 2		NO. 3	NO. 4	CROWN	
	-	AREA	C DEWERIT	TAREA	AREA'S DEWERITAREA'S DEWERIT	AREA-%	DEWERIT	AREA-% DEWE	RIT AREA'S DEME	BRITARE	A-% DEW	ERITAR	A-N DEWER	AREAS DEWERIT AREAS DEWERIT AREAS DEWERIT AREAS DEWERIT AREAS DEWERIT AREAS DEWERIT	AREA'S DEWERIT	ERIT
ž	C 1.00	15	15.00	0.5	50.00				60 60.00	00 70		70.00				
ž	MHC 0.75	25	18.75	30	22.50	2.5	18.75			10		7.50 2	20 15.0	00		
	MC 0.50	09	30.00	20	10.00	ıs	2.50	15 7.50		ro.	-	2.50 1	10 5.0	00		
881	LC 0.25								40 10.	00 5	1.	. 23		10 2.50		
CA	VLC 0.15									-		-		40 6.00		
	CARBON	9	63.75	80	82.50	21.25	25	7.50	70.00	∞	81.25		20.00	8.50		
80	BL 0.100					70	7.00	85 8.50		10		.00	70 7.	00	100 10	00
90	DBrL 0.075													20 1.50	-	
A:	L 0.050											-		-		
JA J	AL 0.025													-		
o ≥	AL 0.010											-				
1	RL 0.001															
	LACQUER					7.	7.00	8.50			1.00		7.00	3.00	10.00	
CLEAN	0 N															
02	ZONAL RATING															
LOCA	LOCATION FACTOR											-				
WEIG	WEIGHTED RATING	-	63.75	∞	82.50	28	28.25	16.00	70.00	00	82.25	-	27.00	11.50	10.00	Γ
1	ATOL OUTHOUGH		04100000							1		1			22.22	7

*WEIGHTED TOTAL DEPOSITS

CRC DIESEL RATING SYSTEM

STANDARD COMPUTATION SHEET FOR PISTON RATING

DATE 4-25-77

30-131703

3-53-5

ENGINE NO. LABORATORY TEST NUMBER 1% S DF-2 RATER E.R. Lyons STAND NO. 2 TEST LABORATORY AFLRI AL-6576 TEST PROCEDURE **LEST HOURS** LUBRICANT

N PISTON NO. 440

NO. 1 GROOVE, VOLUME % PISTON WTD - RATING

AREAN DEMENITAREAN DEMENITAREAN DEMERIT AREAN DEMERITAREAN DEMERITAREAN DEMERITAREAN DEMERITAREAN DEMERITAREAN 10.00 UNDER. 1001 6.50 .50 .125 3.00 NO.A 3.00 20 65 10 5.00 80.00 NO.3 85.00 LANDS 20 65.00 80 2.50 11.25 1.00 NO. 2 78.75 15 10 10 20.00 65 8.75 .50 6.00 34.75 NO. 1 20 35 n 40 5.50 22.50 NO. 4 22.50 22 45 11.25 4.00 5.00 20.00 36.25 NO. 3 40 GROOVES 15 40 37.50 50.00 NO. 2 87.50 20 50 15.00 33.75 15.00 63.75 NO. 1 2 45 AL 0.025 FACTOR 0.10 0.075 0.050 DEPOSIT 0.15 0.75 0.50 0.25 CARBON

*WEIGHTED TOTAL DEPOSITS

10.00

7.125

1.00

.50

20

'n

4.00

0.00

R

LACQUER

10.00

10,125

85.00

79.75

35.25

28.00

40.25

87.50

63,75

WEIGHTED RATING LOCATION FACTOR

ZONAL RATING

CLEAN

VLC

2

CARBON

DBrL

BL

AL

MHC

Y

DEPOSIT

TYPE

MC

CRC DIESEL RATING SYSTEM

STANDARD COMPUTATION SHEET FOR PISTON RATING

PISTON NO.

TEST PROCEDURE 210 LA
TEST HOURS 210 LA
TEST LABORATORY AFLRL STA
LUBRICANT AL-6576 FU

RATER <u>E.R. Lyons</u> DATE <u>4-25-77</u> LABORATORY TEST NUMBER <u>3-53-5</u> STAND NO. <u>2</u> ENGINE NO. <u>3D-131703</u> FUEL 18 S. DF-2

NO. 1 GROOVE, VOLUME-%
PISTON WTD* RATING 487

									State of the same of the same of		NO. OF STREET,			Contraction of the Contraction o	The second second					
						GROO	3VES							7	LANDS				UNDER	ER.
0	DEPOSIT	DEPOSIT	Š	1.0	ž	NO. 2	Z	NO. 3	Z	NO. 4	NO.	-	S	NO. 2	ž	NO. 3	Ž	NO. 4	CROWN	Z.
	2		AREA-%	DEMERIT	AREA-%	AREA-% DEWERIT AREA-% DEMERIT		AREA% DEMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA.%	DEMERIT
	ž	1.8	50	50.00	05 (50.00	15	15.00			35	35.00	7.5	75.00	5.0	50.00				
	MHC	0.75	20	37.50	0 2 0	37.50	2	3.75			5	3.75	2.5	18.75						
NO	S E	0.50					25	12.50			10	5.00			40	20.00				
887	2	0.25					45	11.25	7.5	18.75	50	12.50			10	2.50	0.5	12.50		
70	VLC	0.15					10	1.50									10	1.50		
	3 &	CARBON	87.50	50	87.	.50	4	44.00	18,	18.75	56.	2.5	93.	75	72.50	50	14.00	0.0		
	BL	0.100							2.5	2.50									10	0.00
	DBrL	0.075																		
8E	AL	0.050															5	.125		
Onl	LA LA	0.025															10	.25		
DA.	VAL	0.010																		
7	RL	0.001																		
	7,8	LACQUER							2.	2.50								375	10.00	00
	CLEAN	0																		
	ZONAL	ZONAL RATING																		
-	OCATION	LOCATION FACTOR																		
.5	VEIGHTE	WEIGHTED RATING	87.50	20	87	87.50	4	44.00	21.	.25	56.	25	93.	7.5	72.	50	14.	375	10.00	00
1	The Lotter	STISCOST INTO TOTAL DEBOGITE	41 050	DEITE																

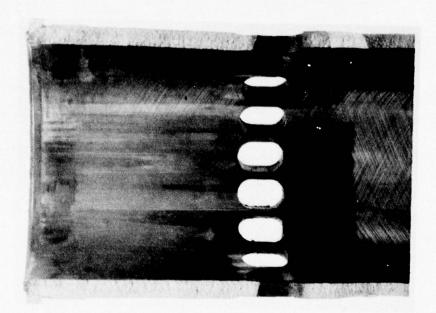
*WEIGHTED TOTAL DEPOSITS

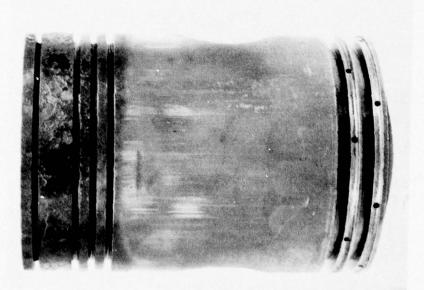
CYLINDER LINER I.D. (IN) TEST #5

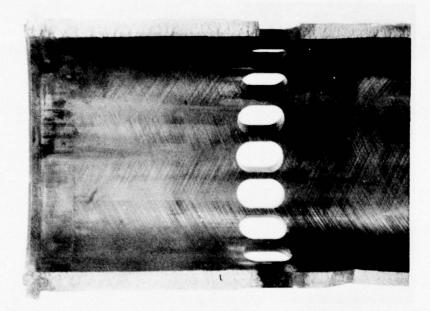
Cv	linder		Front/Back			st/Antith	
	No.	Тор	Middle	Bottom	Top	Middle	Bottom
1.	After Before Δ	$\frac{3.8763}{3.8760}$	$\frac{3.8764}{3.8763}$	$\frac{3.8768}{3.8766}$	$\frac{3.8764}{3.8761}$	$\frac{3.8766}{3.8763}$	$\frac{3.8770}{3.8766}$
2.	After Before Δ	3.8760 3.8756 0.004	$\frac{3.8761}{3.8755}$	$\frac{3.8761}{3.8756}$	3.8755 3.8750 .0005	3.8758 3.8754 .0004	$\frac{3.8760}{3.8756}$
3.	After Before Δ	3.8756 3.8752 .0004	3.8758 3.8754 .0004	3.8758 3.8754 0004	$\frac{3.8756}{3.8751}$ 0005	$\frac{3.8758}{3.8754}$	$\frac{3.8759}{3.8754}$
	rage (All rage T/AT		0.0004 1 0.0004 1	IN .			

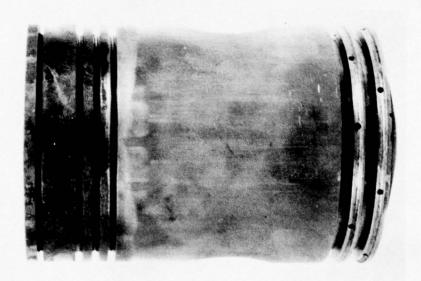
PISTON RING GAP (IN) TEST #5

					Ring	No.			
Pis	ton No.	1		3	4	_ 5	6	7	8
1.	After Before Δ	.035 .034 .001	$031 \\ 033 \\ (002)$	$\begin{array}{c} .033 \\ .033 \\ \hline 0 \end{array}$	0.035 0.036 0.001	$\begin{array}{r} .030 \\ .025 \\ \hline .005 \end{array}$.025 $.023$ $.002$.025 .022 .003	023 020 003
2.	After Before Δ	.044 $.041$ $.003$	$\begin{array}{r} \cdot 032 \\ \cdot 032 \\ \hline 0 \end{array}$	032 033 $(.001)$	$\begin{array}{r} \cdot 032 \\ \cdot 032 \\ \hline 0 \end{array}$	026 024 002	026 024 002	026 024 002	025 023 002
3.	After Before Δ	.039 .035 .004	$\begin{array}{c} .030 \\ .030 \\ \hline 0 \end{array}$	$\begin{array}{c} .031 \\ .031 \\ \hline 0 \end{array}$	$\begin{array}{r} \cdot 032 \\ \cdot 032 \\ \hline 0 \end{array}$.020 .020	.018 $.017$ $.001$	026 023 003	$\begin{array}{r} \cdot 027 \\ \cdot 024 \\ \hline \cdot 003 \end{array}$
Avg	F/R (#1) Wear		0.003	IN				









No. 3 - Thrust Side (Best)

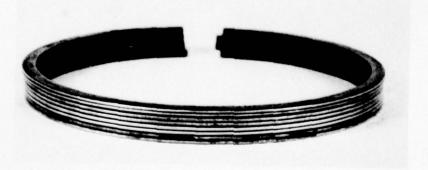
RING FACE CONDITION Test #5



Piston - 1



Piston - 2



Piston - 3

APPENDIX D

3-53 TEST #6

FUEL: 1% S, DF-2

LUBE: AL-6856 (MC-520)

START: 9 May 1977

END: 27 May 1977

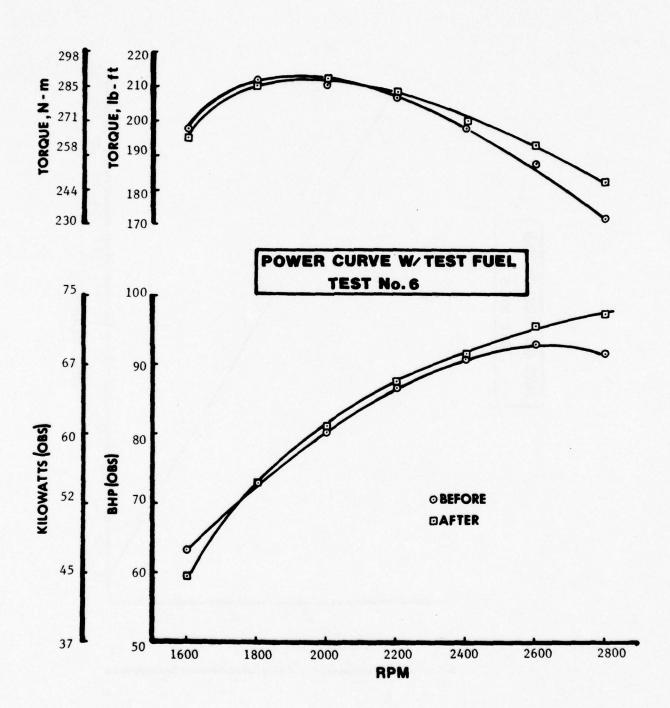
		Power		Id1e
	Min	Max	Avg	(Avg)
Engine Speed, rpm	2797	2806	2801	651
Load, 1bs	97	106	104	
Torque, 1b-ft	170	186	181	
BHp obs	90	99	97	
Fuel Rate, 1b/hr	41.0	44.8	44.1	
BMEP, psi	81	88	86	
BSFC 1b/BHp-hr	0.443	0.468	0.457	
Temperatures, °F				
Jacket Coolant-In	194	196	196	94
Jacket Coolant-Out	204	205	204	100
Oil Sump	248	252	250	
Inlet Air (Blower)	74	86	82	
Exhaust Manifold	950	975	965	
Fuel @ Return	146	151	148	
Pressures				
Oil Gallery, psig	43	45	44	30
Blower Discharge, psig	8.4	8.7	8.6	
Intake Vacuum, in. H ₂ O	7.0	7.1	7.0	
Crankcase, in. H ₂ 0	0.21	0.22	0.22	
Exhaust, Common, in. Hg	2.9	3.1	3.0	



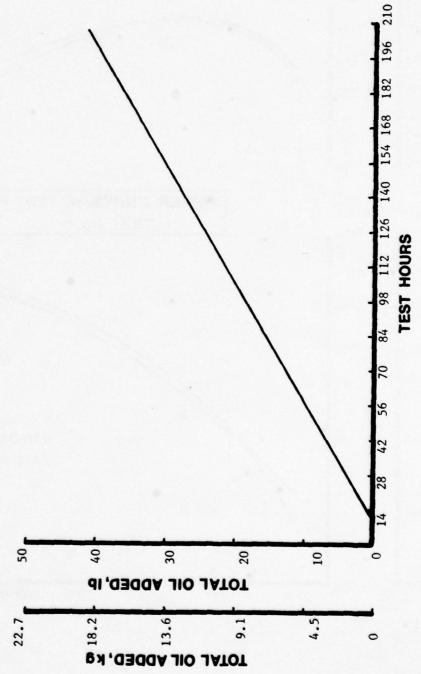
LUBRICANT ANALYSES TEST #6

ASTM Method	New Oil	70 Hrs	140 Hrs	210 Hrs
D445 D445	121.0 12.0	143.7 13.9	164.3 14.9	173.5 15.5
D664 D2896	2.3 13.9	2.9 11.0	3.3 11.1	3.8 12.1
D932	0.04 0.04			0.07 0.01
D287	0.01 25.5			0.83 0.73 24.3
D9 7 D9 2 D5 24	-17 223 2.10	3.01	3.64	221 3.79
D874 Method AA	1.64 < 50	1.77	1.96	2.03
AA AA/XRF	26 .44/.46			
AA XRF	10			19 7 8
AA AA		 70	75	16 < 50 90
	D445 D445 D2270 D664 D2896 D893 D287 D97 D92 D524 D874 Method AA AA/XRF AA AA/XRF AA AA	Method Oil D445 121.0 D445 12.0 D2270 101 D664 2.3 D2896 13.9 D893 0.04 0.03 0.01 D287 25.5 D97 -17 D92 223 D524 2.10 D874 1.64 Method <	Method Oil Hrs D445 121.0 143.7 D445 12.0 13.9 D2270 101 D664 2.3 2.9 D2896 13.9 11.0 D893 0.04 0.03 0.01 D287 25.5 D97 -17 D92 223 D524 2.10 3.01 D874 1.64 1.77 Method AA 26 AA/XRF .44/.46 AA 07/.08 AA 10 XRF AA AA AA AA AA AA	Method Oil Hrs Hrs D445 121.0 143.7 164.3 D445 12.0 13.9 14.9 D2270 101 D664 2.3 2.9 3.3 D2896 13.9 11.0 11.1 D893 0.04 0.03 0.01 D97 -17 D92 223 D524 2.10 3.01 3.64 D874 1.64 1.77 1.96 Method AA 26 AA 26 AA 10 XRF AA 10 XRF AA <t< td=""></t<>

--- = Not Determined.
AA = Atomic Absorption.
XRF = X-Ray Fluorescence.







RING FACE CONDITION: % BURNING TEST #6

		Cylinder Number	r
	1	2	3
First Ring	3	50	2
Second Ring	40	95	90
Third Ring	30	70	50
Fourth Ring	10	50	75
Average of all	48%		

RING STICKING TEST #6

Ring		Piston Number	
No.	1	2	3
1	Sluggish	30% Cold Stuck	Sluggish
2	F	F	F
3	F	F	F
4	F	F	F

F = Free

CYLINDER LINERS TEST #6

		C) Per	Cylinder Liner Scuffing Percent of Compression Ring	scuffing sion Ring		
Cylinder	Percent Port	Percer	Percent Scuffed	% Total		
Number	Restriction	Thrust	Anti-Thrust	Area Scuffed	% Glazed	% Lacquer
1	25	18	30	24	10	06
2	2	S	85	4.5	0	100
8	2	S	5.5	30	0	06
Average	4	6	5.7	33	3	97

3.8720 3.8712 .0008 PISTON O.D. (IN) TEST #6 3.8712 3.8712 Cylinder Before After

3,8718

3.8712

9000.

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PISTON SURFACE CONDITION TEST #6

	Piston Number			
	1	2	3	
Top Land	N	N	N	
Skirt	Lt. Scuff-T. Lt. Scratch	Very Heavy Scratch	Lt. Scuff-AT Lt. Scratch	
Piston Pin	N	N	N	

N = Normal

PISTON GROOVE INSIDE DIAMETER -% RING SUPPORTING CARBON TEST #6

		Piston Number		
Piston Ring	Quadrant	1		3
	1	100	100	95
1	2	0	0	0
	3	0	0	0
	4	0	0	0
	1	0	10	0
2	2	50	0	15
	3	40	100	100
	4	0	20	0

Quadrants:

1 = Thrust

2 = Rear

3 = Anti-thrust 4 = Front

	Cylinder No.			
Area	1	2	3	
Head		A11 90%- AHC		
Face		A11 100%-9		
Tulip		A11 100%-9		
Stem		All Normal		

EXHAUST VALVE SURFACE CONDITIONS TEST #6

		Cylinder No.	
Freeness in Guide	F	F	F
Head	N	N	N
Face	A11 v	ery heavy to heavy	pitting*
Seat	N	N	N
Stem	N	N	N
Tip	N	N	N

N = Normal

F = Free

^{*1} valve each cylinder leaking due to face build-up. Cyl-3 also one valve channeled on face and leaking.

RING DEPOSITS TEST #6

LACQ	0	20-9	70-7	30-3 100-3	000	0 6 1	95-2 10-4	90-2 10-7	90-3 100-4
CARB	100-1/2 AHC	0	0	0	100-1/2 AHC 100-1/2 AHC 100-1/2 AHC	0	0	0	0
LACQ	40-9	30-8	2-8	95-6 100-3	0 0 0 100-9	100-2	50-3	50-4 100-4	100-3
CARB 2	60-1/2 AHC	0	0	0	100-1/2 AHC 100-1/2 AHC 100-1/2 AHC 0	0	0	0	0
LACQ	25-9	40-7	20-4	100-3	0 0 0 100-9	100-2	5-5	95-2 100-3	60-4
CARB	70AHC	0	0	0	100-1/2 AHC 100-1/2 AHC 100-1/2 AHC	0	0	0	0
Number	1	7	8	4	1284	1	2	3	4
Cylinder Number Ring	Top				<u>a</u>	Bottom			

STANDARD COMPUTATION SHEET FOR PISTON RATING ATER E.R. Lyons DATE 6-2-77 3D-131703 3-53-6 2 ENGINE NO. 1% S, DF-2 LABORATORY TEST NUMBER_ STAND NO.

TEST LABORATORY AFLRL LUBRICANT AL-6856 MC 520 TEST HOURS_

TEST PROCEDURE_

FUEL_

PISTON NO. _

NO. 1 GROOVE, VOLUME-%

Public P				MC	520												PISTO	N WTD	PISTON WTD. RATING	٥	452
0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010 0.0010							GRO	OVES							7	LANDS				2	DER.
1.00 0.75 0.25 0.25 0.15 RBON TING 0.005 0.005 0.005 0.005 0.0010 0.0010 0.001	0	EPOSIT	PEPOSIT	S	1.1	Z	0.2	Z	0.3	NO.	4	NO.	-	N	. 2	ž	NO. 3	NO	4.0	CRC	CROWN
1.00 80 80 00 25 75.00 40.00 25 25.00 75 0.75 20 15.00 25 18.75 35 8.75 75 18.75 25 0.25 35 8.75 35 8.75 75 18.75 25 0.25 0.15 61.25 8.75 43.75 81. 0.005 30.05 80.05 <				AREA-%	DEMERIT	AREA-9	W DEMERI	AREA-9	GOEMERIT	AREA-% DE	EMERIT	AREA-% D	EMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA.%	DEMER
0.75 20 5.00 25 18.75 18.75 18.75 18.75 18.75 25 12.50 18.75 25 18.75 26 18.75 27 18.75 27 18.75 27 18.75 28 18.75 28 17 18.75 28 18.75 28 18.75 <th></th> <th>Ä</th> <th>1.00</th> <th></th> <th>80.00</th> <th></th> <th>75.00</th> <th>4</th> <th>40.00</th> <th></th> <th></th> <th>2</th> <th>5.00</th> <th></th> <th>75.00</th> <th>35</th> <th>35.00</th> <th></th> <th></th> <th></th> <th></th>		Ä	1.00		80.00		75.00	4	40.00			2	5.00		75.00	35	35.00				
0.50 25 12.50 8.75 75 18.75 25 0.15 35 8.75 75 18.75 25 0.15 35.75 61.25 8.75 43.75 81. 80.00 93.75 61.25 8.75 43.75 81. 0.005 90.00 93.75 61.25 8.75 43.75 81. 0.050 90.00 93.75 65.50 90.00 90.00 0.00 90		MHC	0.75		15.00	2.5	18.75														
0.25 8.75 35 8.75 35 8.75 18.75 25 0.15 RBON 93.75 61.25 8.75 43.75 81. 7 100 0.100 93.75 61.25 8.75 43.75 81. 0.050 9.005 <th>NO</th> <th></th> <th>0.50</th> <td></td>	NO		0.50																		
0.15 95.00 93.75 61.25 8.75 43.75 81. RBON TING 95.00 93.75 61.25 8.75 43.75 81. 0.100 0.005 0.005 0.005 0.007	986		0.25						7.	5 8	.75			25	6.25	10	2.50	10 2	2.50		
RBON 95.75 61.25 8.75 43.75 81. 0.100 0.100 65.6.50 8.75 81. 0.075 0.075 0.065 0.06	6		0.15																		
0.100 0.075 0.050 0.025 0.010 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001		25	ARBON	. 95.	00	93	.75	9			5	3.	5	81	25	37.	50	2.50	0		
0.075 0.050 0.025 0.010 0.001 0.001 0.08R TING 0		BL	0.100							9 59	2.0					55	5.50	55	5.50	100	10.00
0.050 0.025 0.010 0.001 0.001 TING 0 AATING		DBrL																			
0.025 0.010 0.001 0.001 TING 0 AATING	83	AL																35	.875		
0.001 0.001 TING 0 AATING FACTOR	ino	LAL																			
0.001 0.001 TING 0 AATING FACTOR	DA.	VAL																			
ATING O RATING	<u></u>	R.																			
CLEAN 0 ZONAL RATING LOCATION FACTOR		32	COUER							6.5	0					s.	5.0	6.37	375	10	00
ZONAL RATING LOCATION FACTOR		LEAN																			
LOCATION FACTOR		ZONAL	RATING																		
		OCATION	N FACTOR																		
WEIGHTED RATING 95.00 93.75 61.25 15.25 43.75 81.25	_	VEIGHTE	DRATING	95.	0.0	93	75	9	0	5.2		3.	12			43.00	0.0	8.87	75	10.	00

*WEIGHTED TOTAL DEPOSITS

PISTON NO. STANDARD COMPUTATION SHEET FOR PISTON RATING RATER E.R. Lyons DATE 6-2-77 LABORATORY TEST NUMBER 3-53-6 STAND NO. 2 ENGINE NO. 3D-131703 TEST LABORATORY AFLRI

TEST PROCEDURE_ TEST HOURS_

2 ENGINE NO. 3D-131703 18 S, DF-2 STAND NO.

MC 520

LUBRICANT

464

NO. 1 GROOVE, VOLUME-% PISTON WTD . RATING

-				S L	GHOOVES							4	LANDS				UNDER.	ER.
SIT	NO.	1	S	1.2	ž	5.3	ž	5.4	NO	1.1	NO	1.2	N	.3	Ž	0,4	CRO	Z Z
_	AREA-% D	EMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA-%	EMERIT
	100	00.00	9.0	90.06	2	25.00			80	50.00	80	80.00	5.0	50.00				
5			10	7.50														
0					2.5	12.50												
5					5.0	12.50	35	8.75	5.0	12.50	10	2.50	5.0	12.50	02	7.50		
5																		
	100.00	0	97.	5.0	5.0	00.	∞	. 75	62.	.50	82.	5.0	62	.50	1	.50		
8							65	6.50			10	1.00			45	4.50	100	10.00
375																		
920															2.5	1.25		
25																		
010																		
100																		
æ .g							9	.50			1.	00			5.	. 75	10	10.00
0																		
NG																		
CTOR																		
TING	100.00	0	97.	50	50	00.	15	.25	62.	50	83.	50	62	.50	13.	25	10	00
TYPE TYPE TYPE TYPE TYPE TYPE TYPE TYPE	1.00 1.00 1.00 0.75 0.75 0.75 0.15 0.050	1.00 1.00 1.00 0.75 0.75 0.75 0.15 0.050	1.00 1.00 1.00 0.75 0.75 0.75 0.15 0.050	1.00 1.00 1.00 0.75 0.75 0.75 0.15 0.050	1.00 1.00 1.00 0.75 0.75 0.75 0.15 0.050	PACTOR NO. 1	DEPOSIT NO. 1 NO. 2 FACTOR AREA% DEWERIT AREA% DEWERITARE AND EMERITARE	NO. 1 NO. 2 NO. 3 NO. 4 NO. 1 NO. 2 NO. 3 NO. 4 NO. 4 NO. 4 NO. 5 NO. 3 NO. 4 CFR ABELYA PERENTIAREA-A DEMERNITAREA-A DEM										

STANDARD COMPUTATION SHEET FOR PISTON RATING RATER	ST S
	EST PROCEDURE 210 EST HOURS EST LABORATORY AFLRL UBRICANT MC 520 MC 520 MC 520 MC 0.75 MC 0.75 MC 0.25 MC 0.25 CARBON LC 0.25 CARBON LC 0.25 CARBON LC 0.25 CARBON LC 0.25 LC 0.25 CARBON LC 0.00 BL 0.000 CARBON LAL 0.001 CLEAN 0 ZONAL RATING

WEIGHTED TOTAL DEPOSITS

10.00

21.75

52.625

61.50

43.75

16.00

53.75

66.25

100.00

WEIGHTED RATING

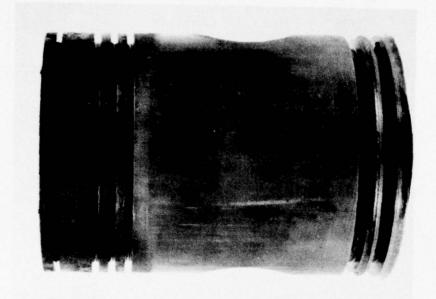
CYLINDER LINER I.D. (IN) TEST #6

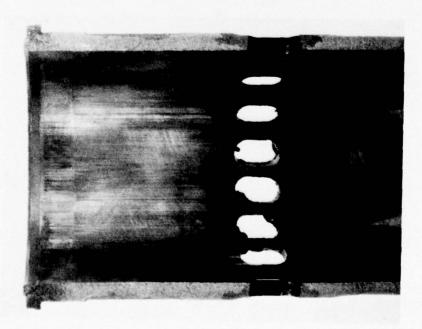
	linder	Paral	ront/Back lel to Cr	ank	Perpend	st/Antithi	Crank
	No.	Тор	<u>Middle</u>	Bottom	Тор	Middle	Bottom
1.	After Before Δ	3.8766 3.8766 0	$\frac{3.8770}{3.8767}$ $\frac{0.0003}{0.0003}$	$\frac{3.8777}{3.8771}$ $\frac{0.0006}{0.0006}$	3.8780 3.8765 0.0015	3.8782 3.8768 0.0014	$\frac{3.8781}{3.8771}$ 0.0010
2.	After Before Δ	3.8766 3.8763 0.0003	$\frac{3.8769}{3.8765}$ $\frac{0.0004}{0.0004}$	$\frac{3.8773}{3.8769}$ $\frac{0.0004}{0.0004}$	$\frac{3.8780}{3.8763}$ $\frac{0.0017}{0.0017}$	3.8786 3.8765 0.0021	$\frac{3.8780}{3.8770}$ $\frac{0.0010}{0.0010}$
3.	After Before A	3.8757 3.8757 0	3.8761 3.8759 0.0002	$\frac{3.8768}{3.8763}$ 0.0005	3.8774 3.8755 0.0009	3.8772 3.8757 0.0015	3.8766 3.8759 0.0007
	rage (All rage T/AT		0.0008 I 0.0013 I				

PISTON RING GAP (IN) TEST #6

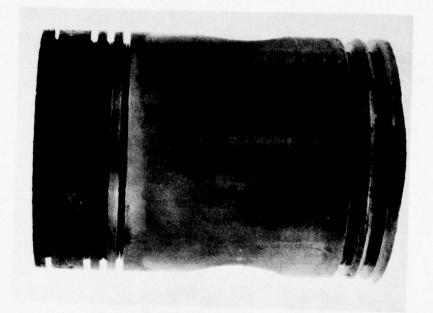
					Ring	No.			
Pis	ton No.	_1		3	4	5	6	7	8
1.	After Before Δ	$0.036 \\ 0.034 \\ \hline .002$	$\begin{array}{c} 0.032 \\ \underline{0.032} \\ 0 \end{array}$	$\begin{array}{c} 0.028 \\ \underline{0.028} \\ 0 \end{array}$	0.027 0.027 0	$0.022 \\ 0.020 \\ \hline .002$	0.023 0.022 0.01	$\frac{0.022}{0.022}$	$\begin{array}{c} 0.022 \\ \underline{0.022} \\ 0 \end{array}$
2.	After Before Δ	$\begin{array}{c} 0.033 \\ \underline{0.033} \\ 0 \end{array}$	$0.035 \\ 0.034 \\ \hline 0.001$	$0.032 \\ 0.032 \\ 0$	$0.028 \\ 0.027 \\ \hline 0.001$	$0.021 \\ 0.020 \\ \hline .001$	0.023 0.022 0.01	$\begin{array}{c} 0.022 \\ 0.022 \\ \hline 0 \end{array}$	0.023 0.022 0.01
3.	After Before A	$0.037 \\ 0.035 \\ \hline .002$	0.025 0.025 0	$\begin{array}{c} 0.025 \\ \underline{0.025} \\ 0 \end{array}$	0.027 0.026 0.001	$0.021 \\ 0.020 \\ \hline .001$	$0.022 \\ 0.021 \\ \hline .001$	$0.022 \\ 0.021 \\ \hline .001$	$\begin{array}{c} 0.021 \\ 0.021 \\ \hline 0 \end{array}$
Ave	F/R (#1) Wear	0.001	IN					

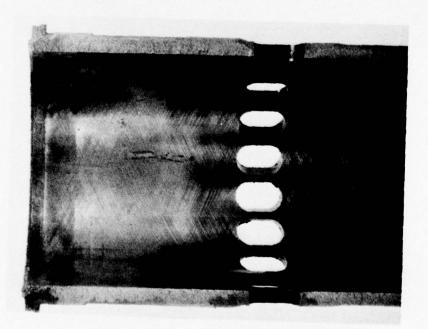
PISTON AND CYLINDER LINER CONDITION Test #6





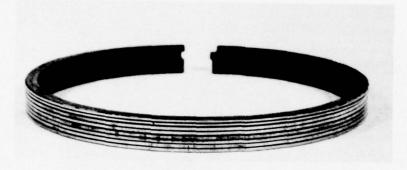
No. 2 Antithrust Side (worst)





No. 2 - Thrust Side (best)

RING FACE CONDITION Test #6



Piston - 1



Piston - 2



Piston - 3

APPENDIX E

3-53 TEST #11

FUEL: 1% S, DF-2

LUBE: AL-6942

START: 29 NOVEMBER 1977

END: 20 DECEMBER 1977

ENGINE OPERATING DATA (AVG) TEST #11

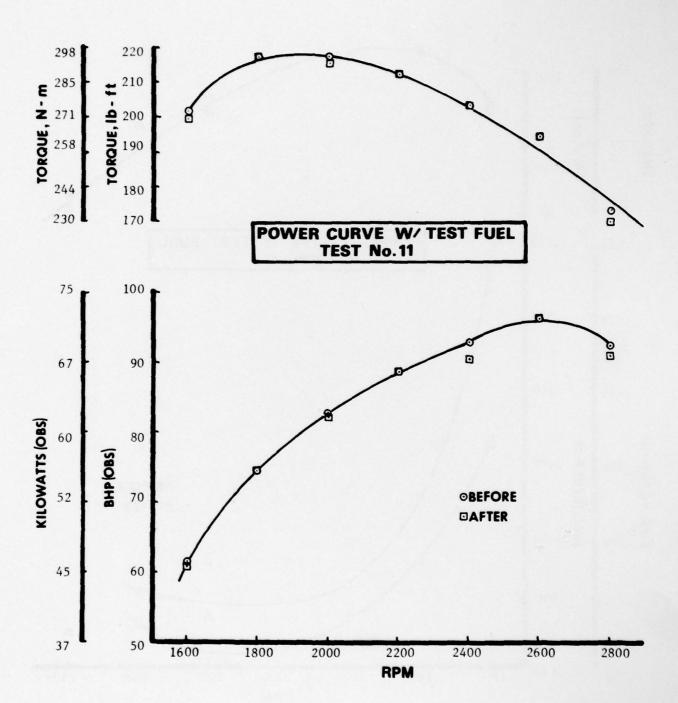
	Min	Power Max	Avg	Idle (Avg)
Engine Speed, rpm Load, 1bs Torque, 1b-ft BHp obs Fuel Rate, 1b/hr	2798 94 165 88 35.6	2803 99 173 92 40.8	2801 97 169 90 39.7	649
BMEP, psi BSFC 1b/BHp-hr Temperatures, °F	78 0.385	82	80 0.441	
Jacket Coolant-In Jacket Coolant-Out Oil Sump Inlet Air (Blower) Exhaust Manifold Fuel @ Return	196 204 240 60 895 138	197 205 248 82 940 149	197 205 244 74 919 144	95 100
Fuel @ Filter Pressures Oil Gallery, psig Blower Discharge, psig Intake Vacuum, in. H ₂ O Crankcase, in. H ₂ O Exhaust, Common, in. Hg	81 45 4.3 6.9 0.28 2.8	94 45 4.6 7.2 0.33 3.0	90 45 4.4 7.0 0.30 2.9	

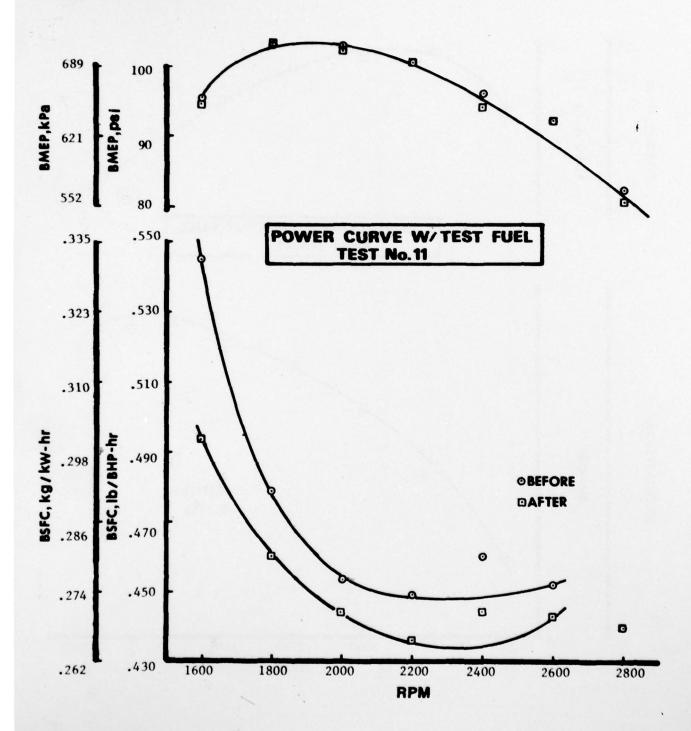


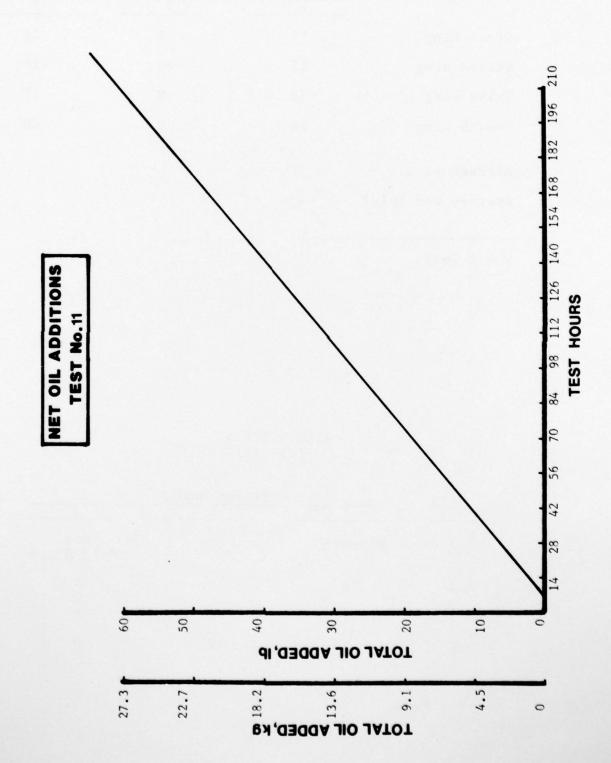
LUBRICANT ANALYSES (AL-6942) TEST #11

Property	ASTM Me thod	New Oil	70 Hrs	140 Hrs	210 Hrs
K. Vis, cS, 40°C K. Vis, cS, 100°C	D445 D445	61.3 10.2	70.1 11.3	74.3 11.7	75.3 11.8
TAN	D2270	153	151	151	151
TBN	D664 D2896	3.7 10.2	3.9 9.2	4.7 9.2	9.2
Insolubles, wt%	D893	10.2	3.2	3.2	3.2
Pentane A		0.09	0.02	0.03	0.03
Benzene A		0.01	0.02	0.02	0.02
Pentane B Benzene B		0.09 0.02	0.03	0.03 0.03	0.03
API Gravity, °	D287	21.9	21.3	21.2	20.8
Pour Point, °C	D97	-41			
Flash Point, °C	D9 2	227	229	232	232
Carbon Residue, wt% Sulfated Ash, wt%	D524 D874	1.53 1.50	1.92 1.59	2.08 1.67	2.14 1.69
Elemental	Method	1.30	1.39	1.07	1.09
Ba, ppm	AA	< 50			
Mg, ppm	AA	11			
Ca, wt% Zn, wt%	AA/XRF AA/XRF	.38/.33	0.38 0.18	0.41 0.19	0.42 0.19
Na, ppm	AA/ AKI	10	0.10	0.19	0.19
Cu, ppm	XRF		6	7	6
Cr, ppm	AA		< 5	< 5	< 5
Pb, ppm Fe, ppm	AA AA/XRF		8 50/40	12 57/60	11 61/60
. , pp	MAY ANT		30/40	37700	01/00

^{--- =} Not Determined.
AA = Atomic Absorption.
XRF = X-Ray Fluorescence.







RING FACE CONDITION: % BURNING TEST #11

		Cylinder Number	
		2	3
First Ring	15	5	25
Second Ring	15	25	20
Third Ring	50	N	75
Fourth Ring	55	10	80
Average of all	31%		
Average w/o Cy1-2	42%		

N = Normal

RING STICKING TEST #11

Ring No.		Piston Numbe	r
NO.		2	3
1	Sluggish	F	80% Cold Stuck
2	F	F	F
3	F	F	F
4	F	F	F

F = Free

CYLINDER LINERS TEST #11

% Lacquer 95 86 100 100 % Glazed 0 7 0 2 Area Scuffed % Total Cylinder Liner Scuffing
Percent of Compression Ring
Travel Area
Percent Scuffed
Thrust Anti-Thrust
Area Scuf 13 26 20 45 38 30 2 80 13 10 20 10 Percent Port Restriction < 1 < 1 × < 1 × Cylinder Number Average

PISTON O.D. (IN) TEST #11

3	3.8715	3.8715	0
2	3.8705	3.8700	.0005
	3.8715	3.8715	0
Cylinder	Before	After	۵

PISTON SURFACE CONDITION TEST #11

		Piston Number	
Top Land		2	3
	N	N	N
Skirt	10% plate melt-T. 5% plate melt-AT. Lt. Scratch	15% plate melt-T. Lt. Scratch	N
Piston Pin	N	N	N

PISTON GROOVE INSIDE DIAMETER - % RING SUPPORTING CARBON TEST #11

Piston Ring	Quadrant	<u></u>	Piston Numb	er
1	1	15	0	5
	2	75	0	45
	3	70	15	0
	4	0	5	25
2	1	5	90	0
	2	10	0	0
	3	80	0	0
	4	5	0	0

Quadrants:

1 = Thrust

2 = Rear

3 = Anti-thrust 4 = Front

EXHAUST VALVE DEPOSITS TEST #11

	Cylinder No.
Area	_123_
Head	All 65%-AHC to Soot, Heavier Than Usual
Face	All Heavy Deposit
Tulip	All Heavier Deposit Than Usual
Stem	All 100%-9 to Clean

EXHAUST VALVE SURFACE CONDITIONS TEST #11

		Cylinder No.	
			3
Freeness in Guide	F	F	F
Head	N	N	N
Face	*	*	*
Seat	N	N	N
Stem	N	N	N
Tip	N	N	N

^{*}Heavier deposit than normal, some leak marks appearing.

RING DEPOSITS TEST #11

Cylinder Number Piston	Number	CARB	LACO	CARB 2	LACO	CARB	LACO
Top	1	20-1/2 AHC	30-6	80-AHC	0	30-AHC	5-9, 55-5
	2	0	25-9	20-1/2 AHC 0	20-9	0	15-9
	84	0	50-6, 25-5 100-6 100-3	0 0	20-8, 60-7 100-5 100-2	00	25-7, 60-6 100-6 100-2
1D	7351	100-AHC 100-AHC 100-1/2 AHC	0000	100-1/2 AHC 100-1/2 AHC 100-1/2 AHC	0	100-1/2 AHC 100-AHC 100-1/2 AHC	0 0 0
Bottom	1	0	100-2	0 0	30-8, 20-7	0 0	100-0
	2	0	30-7	0	25-4, 25-5 50-6	0	50-4 50-4
	3	0	100-2	0	100-3	0	20-3
	4	0	100-2	0	100-2	0	80-3 100-3

STANDARD COMPUTATION SHEET FOR PISTON RATING

RATER E.R. Lyons DATE 12-21-77 LABORATORY TEST NUMBER 3-53-11 STAND NO. 2 ENGINE NO. 3D-131703 FUEL 18S DF-2

TEST HOURS 210 TEST LABORATORY AFLRI AL-6942

LUBRICANT

TEST PROCEDURE_

PISTON NO.

PISTON WTD* RATING 446 NO. 1 GROOVE, VOLUME-%

							1		The second secon		Section of the sectio			The second second second	1					0++
L						GROOVES	NES							LA	LANDS				2	UNDER.
<u> </u>	DEPOSIT	DEPOSIT	NO.		ž	NO. 2	Ž	NO. 3	ž	NO. 4	NO. 1	1.	N	NO. 2	N	NO. 3	ž	NO. 4	CR	CROWN
	2		AREA-%	DEMERIT	AREA-%	AREA-% DEMERIT AREA-% DEMERIT		DEMERIT	AREA-%	AREA% DEMERIT AREA% DEMERIT AREA% DEMERIT AREA% DEMERIT AREA% DEMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA-%		AREA-%	AREA.% DEMERIT AREA.% DEMERIT	AREA-%	DEMERIT
	2	1.00	100	100.0 80	80	80.00					80	80.00	85	85.00						
	MHC	0.75			20	15.0					15	11.25	10	7.50						
NO	S S	0:20																		
887	2	0.25					50	12.50 60	09	15.00	2	1.25	5	1.25	20	2.00				
95	VLC	0.15					30	4.50												
	25	CARBON	100.00	0.0	95.	95.00	17.	17.00	15	15.00	92.50	50	93,75	7.5	5.	5.00				
	BL	0.100					20	2.00	_						7.0	7.00	09	00.9		
	DBrL	0.075							40	3.00									100	7.50
83	R AL	0.050													5	.25	20	1.00		
סחנ	LAL	0.025													5	.125	20	.50		
AC	VAL	0.010																		
1_	RL	0.001																		
	72	LACQUER					2	2.00	3	3.00					7.	7.38	7.	7.50	- 4	7.50
0	CLEAN	0																		
	ZONAL	ZONAL RATING																		
	OCATIO	LOCATION FACTOR																		
5	VEIGHTE	WEIGHTED RATING	100.00	00	95.	95.00	19	19.00	18	18.00	92.	92.50	93.75	7.5	12.38	38	7.	7.50	7.	7.50
]																				

*WEIGHTED TOTAL DEPOSITS

STANDARD COMPUTATION SHEET FOR PISTON RATING

RATER E.R. Lyons DATE 12-21-77
LABORATORY TEST NUMBER 3-53-11
STAND NO. 2 ENGINE NO. 3D-131703
FUEL 18 S DF-2 AL-6942 TEST LABORATORY AFLRL TEST PROCEDURE_

TEST HOURS

LUBRICANT

PISTON NO.

NO. 1 GROOVE, VOLUME-% PISTON WTO - RATING

NO.3 NO.4 NO.1 NO.2 NO.3 NO.4 CRO	L						GROO	VES							1	SONA					
HC 1.00 50 50.00 80 80.00 HC 1.00 50 50.00 80 80.00 MHC 0.75 50 12.50 CARBON 62.50 95.00 RATING CARBON 62.50 95.00	-	TVDE	DEPOSIT	ž	1.0	N	3.2		9.3	S S	4	NO.	-	S	1	S	6	2	4	55	NA.
HG 1.00 50 50 . 00 80 80 . 00 15 . 00 50 15 . 0				AREA-%	DEMERIT	AREA-%	DEMERIT		DEMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA.%	DEMERIT	AREA-%	DEMERIT	AREA.%	DEMERIT	AREA-%	DEMERIT
MHC 0.75 0.26 15.00 50 17.50 10.50 15.00 15.	_	ž	1.00		50.00								25.00	45	15 00						
Machine 0.50 Machine Machine						20			37.50					2.0	15.00						
C 0.35 S 12.50 S 12.50 S 12.50 S S 12.50 S S S S S S S S S	NO		0.50																		
CARBON 62.50 95.00 50.00 43.75 65.00 25.00			0.25	50					12.50	2.0	5.00			2.0		100	75 00				
CARBON 62.50 95.00 50.00 5.00 43.75 65.00 25.00 7.00 BL 0.100 80 8.00 15 1.50 50 5.00 100 AL 0.050 9.00 9.00 9.00 95.00 <th></th> <th>_</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th>															_						
BL 0.100 80 8.00 15 1.50 50 5.00 AL 0.050 AL 0.050 AL 0.050 AL 0.010 AL 0.010 AL		25	ARBON	62.	50	95	00.	20	00.	2	00.	43.	. 75	65	00.	25.	00.				
DBr 0.075		BL	0.100								8.00			15	1.50			50	5.00		
AL 0.050		DBrL																		100	7.50
LAL 0.025	83		0.060															20	1.00		
NI	110	_	0.025															30	. 75		
RAL 0.001	JA.	WAL																			
8.00 1.50 6.75 8.00 1.50 6.75 62.50 95.00 50.00 13.00 43.75 66.50 25.00 6.75	<u></u>		0.001																		
62.50 95.00 50.00 13.00 43.75 66.50 25.00 6.75		7,8	ATING							80	00.			7	.50			6.	75	7	50
62.50 95.00 50.00 13.00 43.75 66.50 25.00 6.75	لــــ	CLEAN																			
62.50 95.00 50.00 13.00 43.75 66.50 25.00 6.75		ZONAL	RATING																		
62.50 95.00 50.00 13.00 43.75 66.50 25.00 6.75		LOCATIO	N FACTOR																		
	-	WEIGHTE	DRATING	62.	50	95	00.	50	00.	13	00	43	75	99	50	25.	00	9	75	7	05

STANDARD COMPUTATION SHEET FOR PISTON RATING

TEST PROCEDURE 210
TEST HOURS 210
TEST LABORATORY AFLRL
LUBRICANT AL-6942

 RATER
 E. R. Lyons
 DATE
 12-21-77

 LABORATORY TEST NUMBER
 3-53-11

 STAND NO.
 2
 ENGINE NO.
 3D-131703

 FUEL
 1% S DF-2

NO. 1 GROOVE, VOLUME:% PISTON WTD* RATING 363

2

PISTON NO.

	The latest lates	-	-		-					-	-	The same of the same of	-	-	The second second	The second second	The second second second			
_					9	GROOV	/ES							37	LANDS				UNDER	خه
ō _	TYPE	DEPOSIT	NO. 1		NO. 2		NO. 3	3	NO. 4	4	NO. 1	1.1	N	NO. 2	N	NO. 3	NO	4	CROWN	-
			AREA-% DEM	ERITARE	A-% DE	WERITA	REA-% D	EMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA.%	EMERIT	AREA % DEMERITAREA % DEMERITAREA % DEWERIT AREA % DEMERITAREA % DEMERITA	ERIT
	ž	1.00	100 10	100.00	30 30	00.0					5.0	50.00	0.6	90.00						
	MHC	0.75)	_	1							1							
NO	MC MC	0.50			20 10	0.0	40	20.00												
BRA	27	0.25			50 12	5					5.0	12.50	10	2.50	10	2.50				
97	VLC	0.15																		
	25	CARBON	100.00		52.50	0	20.00	00			62.	62.50	92.50	50	2.50	0				
	BL	0.100					09	6.00							8.0	8.00	25 2	2.50		
	DBrL	0.075							30	2.25					10	.75			100 7.50	50
83	AL	0.050							7.0	2 50							10	.50	1	
סחו	OO LAL	0.025			_					00.0							65 1	1.625		
AC	VAL	0.010			-															
1	RL	0.001																		
	1. A.	LACOUER					6.00	00	5.7	75					8.75	5	4.625	10	7.50	
0	CLEAN	0																	_	
	ZONAL	ZONAL RATING																		
3	DCATION	LOCATION FACTOR																		
3	EIGHTEC	WEIGHTED RATING	100.00		52.50	0	26.00	00	5.75	S	62.50	50	92.50	50	11.25	5	4.625	10	7.50	

*WEIGHTED TOTAL DEPOSITS

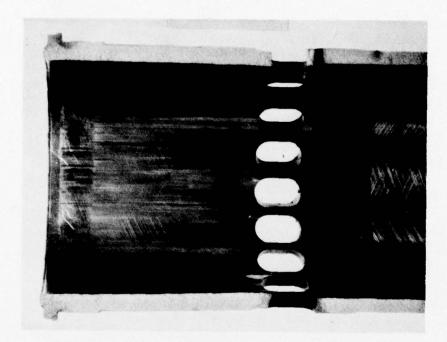
CYLINDER LINER I.D. (IN) TEST #11

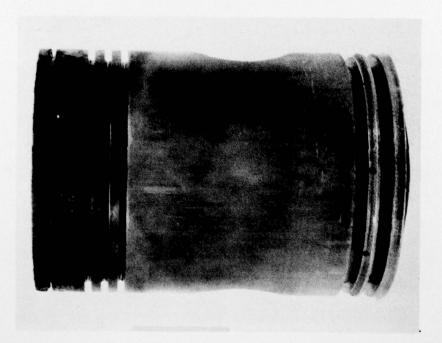
Cv	linder		Front/Bac			st/Antith	
	No.	Тор	Middle	Bottom	Top	Middle	Bottom
1.	After Before Δ	$\frac{3.8767}{3.8761}$ 0006	3.8768 3.8762 .0006	3.8772 3.8764 .0008	3.8769 3.8759 .0010	3.8770 3.8758 .0012	3.8770 3.8762 .0008
2.	After Before A	$\frac{3.8770}{3.8761}$	$\frac{3.8768}{3.8761}$	$\frac{3.8771}{3.8764}$ $\frac{0007}{0007}$	3.8768 3.8760 .0008	$\frac{3.8771}{3.8761}$ $\frac{0010}{0010}$	$\frac{3.8772}{3.8763}$ $\frac{0009}{0009}$
3.	After Before Δ	3.8765 3.8757 .0008	$\frac{3.8766}{3.8759} \\ \hline .0007$	$\frac{3.8769}{3.8762}$	3.8769 3.8758 .0011	$\frac{3.8774}{3.8760}$	$\frac{3.8770}{3.8761}$
	rage (All			IN IN			

PISTON RING GAP (IN) TEST #11

					Ring	No.			
Pis	ton No.	1		3	4	5	6	7_	8
1.	After Before A	0.042 .035 .007	0.040	0.031 0.030 0.001	0.037 0.036 0.001	0.030	0.028 .023 .005	$\frac{0.028}{.023}$	0.030
2.	After Before Δ	0.046 0.035 0.011	0.031	0.027	0.033 0.032 0.001	0.025 .021 .004	0.025 .020 .005	0.025 0.021 0.04	0.025 0.021 0.04
3.	After Before A	0.038 0.031 0.07	0.029 0.029	0.028	0.028	0.028	$0.028 \\ 0.022 \\ \hline 0.006$	0.028 .022 .006	$\frac{0.028}{.023}$
Avg	F/R (#1) Wear	0.00 8	IN					

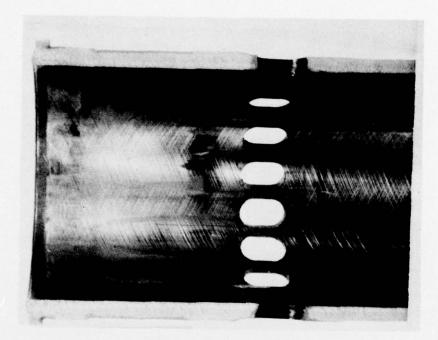
PISTON AND CYLINDER LINER CONDITION Test #11

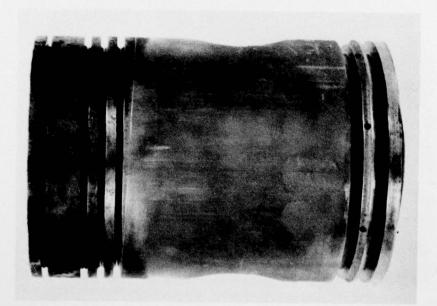




No. 3 - Antithrust Side (worst)

PISTON AND CYLINDER LINER CONDITION Test #11





No. 2 - Antithrust Side (best)

RING FACE CONDITION Test #11



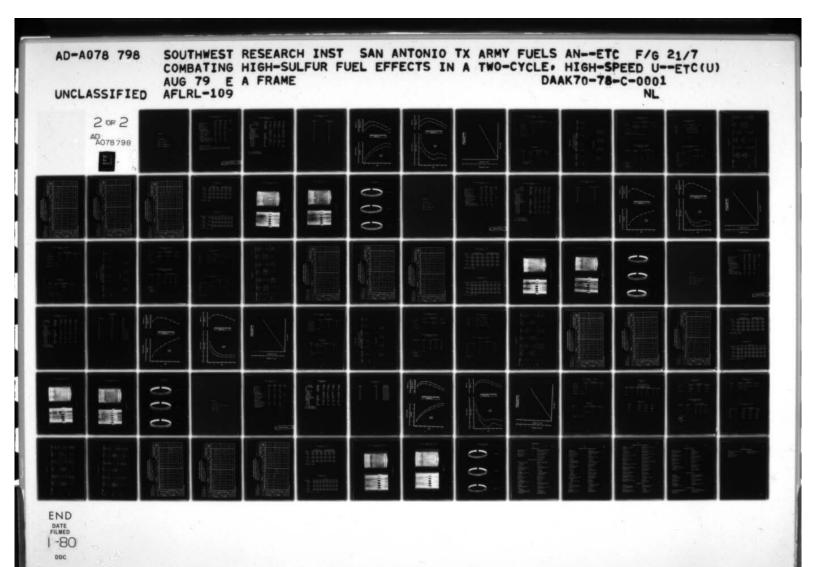
Piston - 1

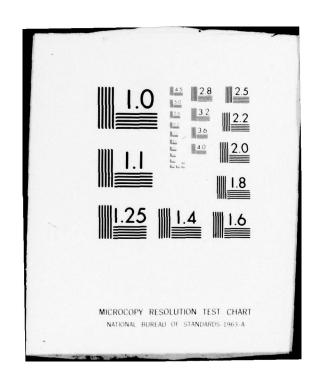


Piston - 2



Piston - 3





APPENDIX F

3-53 TEST #13

FUEL: 1% S, DF-2

LUBE: AL-7135-L

START: 6 FEBRUARY 1978

END: 24 FEBRUARY 1978

ENGINE OPERATING DATA (AVG) TEST #13

		Power		Id1e
	Min	Max	Avg	(Avg)
Engine Speed, rpm	2800	2803	2801	651
Load, 1bs	96	103	100	
Torque, 1b-ft	168	180	175	
BHp obs	89.6	96.2	93.5	
Fuel Rate, 1b/hr	39.2	41.6	40.5	
BMEP, psi	80	86	83	
BSFC 1b/BHp-hr	0.420	0.448	0.433	
Temperatures, °F				
Jacket Coolant-In	197	197	197	95
Jacket Coolant-Out	205	205	205	100
Oil Sump	240	246	243	
Inlet Air (Blower)	72	91	83	
Exhaust Manifold	920	950	935	
Fuel @ Filter	86	94	90	
Fuel @ Return	138	147	143	
Pressures				
Oil Gallery, psig	44	45	44	
Blower Discharge, psig	4.3	4.4	4.4	
Intake Vacuum, in. H ₂ 0	6.5	6.6	6.5	
Exhaust, Common, in. Hg	2.5	3.1	2.8	
Crankcase, in. H ₂ 0	0.31	0.36	0.33	

General Observations:

Cylinder No. 2, lower half connecting rod bearing showed errosion of material. Cylinder No. 2, piston pin bushing showed distress.



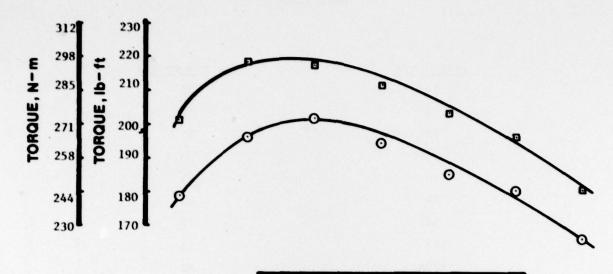
LUBRICANT ANALYSES (AL-7135-L) TEST #13

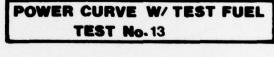
Property	ASTM Method	New Oil	70 Hrs	140 Hrs	210 Hrs
K. Vis, cS, 40°C	D445	67.5	69.6	71.2	71.0
K. Vis, cS, 100°C	D445	9.96	10.38	10.45	10.52
VI	D2270	143	135	133	135
TAN	D664	2.5	3.3	3.5	3.6
TBN	D2896	7.9	6.5	4.7	4.6
Insolubles, wt%	D893				
Pentane A		0.03			0.04
Benzene A		0.01			0.26
Pentane B		0.01			0.03
Benzene B		0.01			0.23
API Gravity, °	D287	18.4			18.0
Pour Point, °C	D9 7	- 34			
Flash Point, °C	D9 2	227	263	265	260
Carbon Residue, wt%	D5 24	1.12	1.57	1.75	1.82
Sulfated Ash, wt%	D874	1.02	1.04	1.05	1.06
Elemental	Method				
Ba, ppm	AA	< 50			
Mg, w%	AA	0.08			
Ca, wt%	XRF	0.09	0.08	0.09	0.09
Zn, wt%	AA	0.13	0.11	0.115	0.115
Na, ppm	AA	< 10			
Cu, ppm	AA		< 1	< 1	< 1
Cr, ppm	AA		< 1	< 1	< 1
Pb, ppm	AA,		7	12	16
Fe, ppm	AA/xrf		53	74	87/95

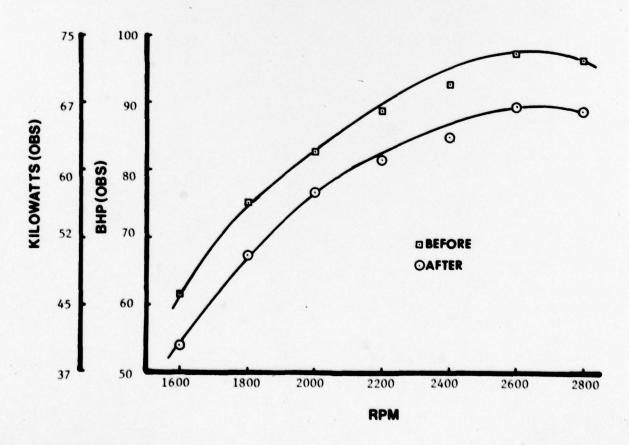
--- = Not Determined AA = Atomic Absorption XRF = X-Ray Fluorescence

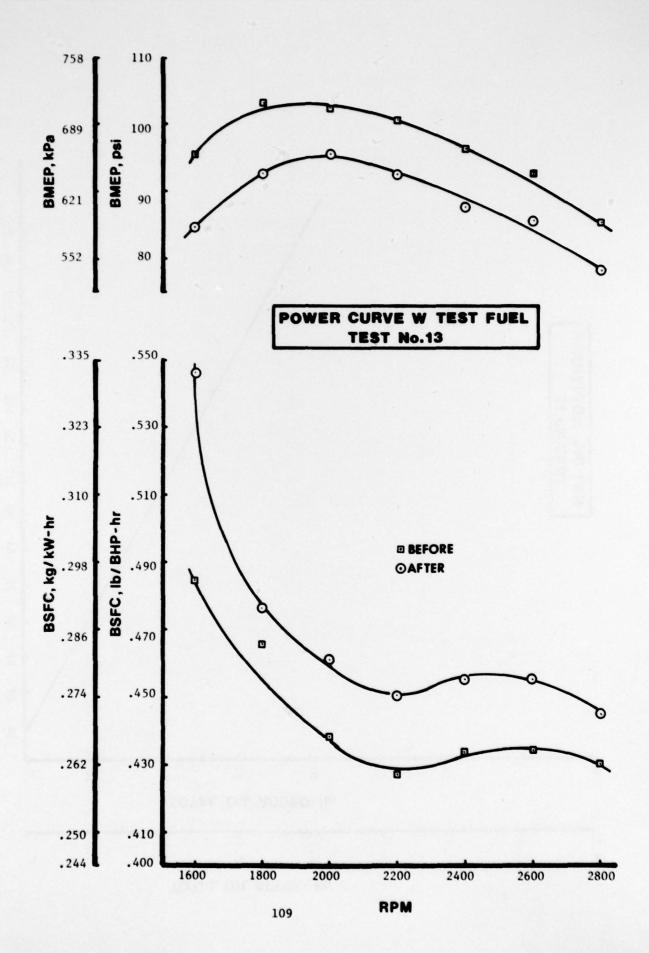
DAILY IRON CONTENT OF USED OIL Test #13

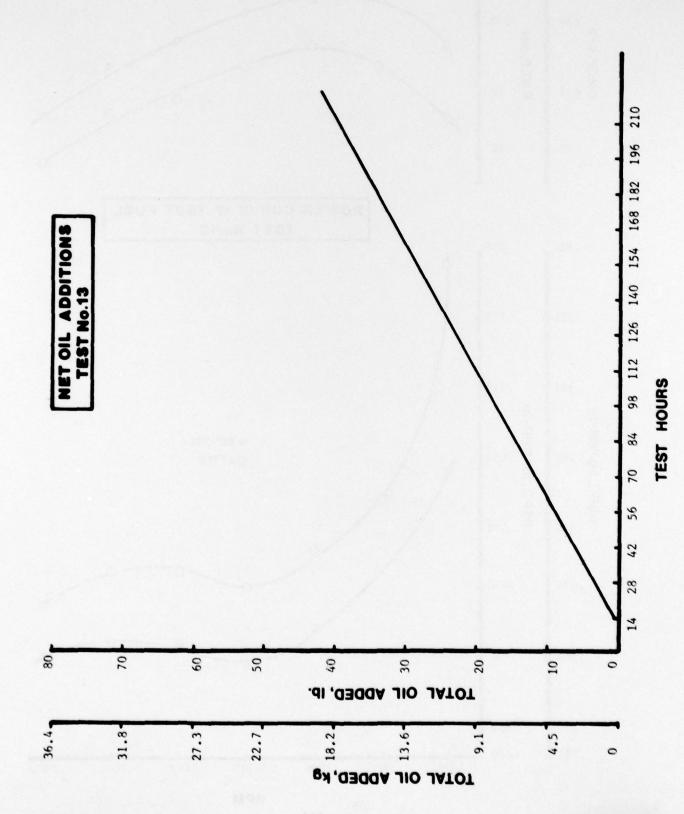
Test Hours	Fe, ppm by XRF
14	35
28	50
42	55
56	60
70	65
84	60
98	72
112	72
126	82
140	75
154	95
168	100
182	90
196	90
210	95











RING FACE CONDITION: % BURNING TEST #13

Cylinder Number		
1	2	3
10	15	5
5	15	15
15	15	5
10	15	5
11%		
	1 10 5 15 10	5 15 15 15 10 15

N = Normal

RING STICKING TEST #13

Ring No.	Piston Number			
	1	2	3	
1	90% HS	100% HS	100% HS	
2	10% S	10% S	F	
3	F	F	F	
4	F	F	F	

HS = Hot Stuck S = Sluggish F = Free

CYLINDER LINERS TEST #13

		\$ Lacquer	06	97	95	16
		% Glazed	10	3	S	۱۰
scuffing sion Ring	f Total	Area Scuffed	17	42	25	2.8
ip ip	Percent Scuffed	Anti-Thrust	15	7.5	35	42
Cylii Percen	Percer	Thrust	20	10	15	15
	Percent Port	Restriction	2	10	ın	7
	Cylinder	Number	1	2	8	Average

PISTON 0.D. (IN) TEST #13

3	3.8710	3.8713		+0.0003
2	3.8710	3.8707		-0.0003
1	3.8710	3.8704		-0.0006
Cylinder	Before	After		٧

PISTON SURFACE CONDITION TEST #13

		Piston Number	
	1	2	3
Top Land	N	N	N
Skirt	Lt. Scratches Lt. Plate Melt T-Side	Lt. to Hvy. Scratches	Lt. Scratches
Piston Pin	N	N	N

N = Normal

No. 2 piston pin bushing showing distress.

PISTON GROOVE INSIDE DIAMETER - % RING SUPPORTING CARBON TEST #13

		P	iston Number	r
Piston Ring	Quadrant	1		3
	1			
1	2			
	3		A11 100	
	4			
	1	10	10	0
2	2	15	0	0
	3	75	5	70
	4	15	0	0

Quadrants:

1 = Thrust

2 = Rear

3 = Anti-thrust

4 = Front

EXHAUST VALVE DEPOSITS TEST #13

	Cylinder No.
Area	
Head	All 90% AHC, 10% soot
Face	All 100%-9 to clean
Tulip	All 1/2 AHC to Lacq-9
Stem	All 1/2 AHC to Lacq-9

EXHAUST VALVE SURFACE CONDITIONS TEST #13

		Cylinder No.	
	1	_2_	3
Freeness in Guide	F	F	F
Head	N	N	N
Face	A11	some light pittin	g
Seat	N	N	N
Stem	N	N	N
Tip	N	N	N

F = Free N = Normal

RING DEPOSITS TEST #13

LACQ	ND 10-7 15-8 10-7 90-5 100-3	0 0 8-06 60-8	ND 90-6 10-3 10-7 80-4, 10-6
CARB	ND 75-1/2 AHC 0	ND 25-AHC 75-1/2 AHC 10-1/2 AHC 40-1/2 AHC	0 0 0
LACQ	ND 0 70-6 30-3 100-4	ND 0 0 100-8	ND 100-6 20-4 80-3 100-3
CARB	ND 85-AHC 15-1/2 AHC 0	ND 90-AHC 10-1/2 AHC 100-1/2 AHC	Q 0 0 0
LACQ	ND 0 15-8 35-5 90-3	0 0 0 0 0 0 0	ND 100-3 20-6 80-4 100-4
CARB	ND 30-AHC 70-1/2 AHC 10-AHC 40-1/2 AHC 10-1/2 AHC	ND 5-RS 20-AHC 75-1/2 AHC 20-AHC 80-1/2 AHC 10-1/2 AHC	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
Number	11 * 2 5 4	12 8 4	1 2 2 4 4
Cylinder Number Ring	Тор	01	Bottom

*ND = Not Determined - Fire ring not removed from piston.

STANDARD COMPUTATION SHEET FOR PISTON RATING

DATE 2 March 1978 3D-131703 LABORATORY TEST NUMBER 703-13 STAND NO. 2 ENGINE NO. FUEL 18 S, DF-2 RATER E. R. Lyons FUEL

TEST LABORATORY AFLRL

LUBRICANT

TEST HOURS 210 TEST PROCEDURE

534

NO. 1 GROOVE, VOLUME-% PISTON WTD . RATING

PISTON NO.

AREA-% DEWERIT AREA-% DEMERIT AREA-% DEMERIT AREA-% DEMERIT AREA-% DEMERIT AREA-% DEMERIT AREA-% DEMERIT AREA-100 10.00 CROWN 10.00 15.00 6.0 4.0 21.00 09 40 5.0 60 60.0 10.0 NO.W 75.00 20 20 LANDS 2.50 90 90.0 92.50 NO. 2 10 20.00 15.00 25.00 NO. 1 80 20 7.50 10.00 25.00 NO. 4 50 9 40 80 80.0 10.0 NO. 3 90.00 20 GROOVES 5.0 90.0 NO. 2 95.00 90 10 100.0 100.00 NO. 1 100 0.010 DEPOSIT 0.100 0.075 0.050 0.025 FACTOR 0.00 0.15 ZONAL RATING 8 0.75 0.50 0.25 LACQUER CARBON 0 FECOUER DBrL MHC VLC CLEAN R DEPOSIT 2 ž 2 AL BL TYPE

WEIGHTED TOTAL DEPOSITS

10.00

21.00

75.00

92.50

25.00

25.00

90.00

95.00

100.00

WEIGHTED RATING LOCATION FACTOR

CARBON

STANDARD COMPUTATION SHEET FOR PISTON RATING RATER E.R. Lyons DATE 2 March 1978 LABORATORY TEST NUMBER 703-13
STAND NO. 2 ENGINE NO. 3D-131703
FUEL 18 S. DE-2

PISTON NO.

NO. I GROOVE, VOLUME &	
PISTON WTD . RATING	488

L	-					GROC	GROOVES							LA	LANDS				1	0300
930	DEPOSIT DE	DEPOSIT	1						0.3	1	3			1	1	5			CROWN	MN
-	-	FACTOR	NO. 1	-	ž	NO. 2		NO. 3	NO. 4	4	NO.	-	ž	NO. 2	ž	NO.3	Z	NO. 4	25	2
			AREA-%	EMERIT	AREA-%	DEMERIT	AREA.	AREA-% DEMERIT	AREA-%	DEMERIT	AREA.%	DEMERIT	AREA.%	DEMERIT	AREA-%	DEMERIT	AREA.%	AREA'S DEMERIT AREA'S DEMERIT	AREA.%	DEMERIT
	£	1.00	100	100.0	06	0.06					10	10.00	06	0.06						
	MHC	0.75			10	7.50	40	30.0							7.5	56.23	20	15.00		
	NC O	0.50																		
887	2	0.25					10	2.50	100	25.0	9.0	22.50	10	2.50			40	10.00		
/ 3	VLC 0	0.15					50	7.50							25	3.75	40	6.00		
	CARBON	BON	100.00	00	97.	50	4(40.00	25.00	0.0	32.50	50	6	92.50)9	60.00	31	31.00		
	91 0	0.100																	100	10.00
_	DBrL	0.075																		
8		0.050																		
ino	141 141	0.025																		
O∀.		0.010																		
1		0.001																		
	LACQUER	ING																	10	10.00
ರ	CLEAN	0																		
	ZONAL RATING	TING																		
3	LOCATION FACTOR	ACTOR																		
×	WEIGHTED RATING	PATING	100 00	00	97	97.50	4	00.0	25.00	00	32.50	5.0	6	92.50	9	60.00	31	31.00	10	10.00

*WEIGHTED TOTAL DEPOSITS

STANDARD COMPUTATION SHEET FOR PISTON RATING

RATER E.R. Lyons DATE 2 March 1978 LABORATORY TEST NUMBER 703-13 703 STAND NO. 2 ENGINE NO. 3D-131703 FUEL 18 S. DF-2

TEST HOURS 210 AFLRL TEST LABORATORY AL-7135

TEST PROCEDURE_

PISTON NO. 3

NO. 1 GROOVE, VOLUME-%
PISTON WTD* RATING 407

DEPOSIT DEPOSIT TYPE FACTOR HC 1.00				20000	3												5	ONDER.
				,										•		South Control of the	1	
+	ž	NO. 1	ž	NO. 2	S	NO. 3	8	NO. 4	NO. 1	-	N	NO. 2	S	NO.3	NO.	.4	CR	CROWN
+-	AREA-%	DEMERIT	AREA-%	AREA-X DEWERIT AREA-X	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA-%	DEMERI
	100	100.0	85	85.0					25	25.0	80	80.0						
MHC 0.75			15	11.23														
MC 0.50					20	10.0	20	10.0	10	5.00			10	5.00				
LC 0.25					80	20.02	40	10.0	65	16.23	20	5.00						
VLC 0.15							20	3.00					75	11.2	20	3.00		
CARBON	10	00.0	86	.25	30.	00	23.	00.	46.	25	85.	00	16.	25	3.0	00		
BL 0.100															20	2.00	100	10.00
DBrL 0.075													15	1.12				
AL 0.050							20	1.00							90	3.00		
0.025																		
L 0.010																		
RL 0.001																		
LACQUER								00.					1	.125	5.0	0.0	10	10.00
CLEAN 0																		
ZONAL RATING																		
LOCATION FACTOR																		
WEIGHTED RATING		0.00	86	.25	30.	00	24	00	46.	25	85	00	17	375	8,0	00	10	10.00
	CARBON RATING BL 0.100 DBrL 0.075 DBrL 0.075 COLAL 0.025 COLAL 0.001 LACQUER RATING CLEAN 0 ZONAL RATING LGCATION FACTOR	0.100 0.075 0.050 0.050 0.025 0.010 0.010 0.010 0.010 0.010 0.010 0.010 0.010	0.100 00 0.100 00 0.100 00 0.100 0.005 0.0050 0.0050 0.0050 0.001	0.000 100.00 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.001	0.100 0.075 0.075 0.050 0.025 0.010 0.010 0.010 0.010 0.010 0.010 0.010 0.010	ATING 0.100 0.075 0.050 0.025 0.001	0.000 100.00 0.005 0.005 0.005 0.005 0.005 0.005 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.000 0.001 0.000	RBON VING 100.00 86.25 30.00 2 0.100 0.075 20 20 0.050 20 20 20 0.025 20 20 0.001 20 20 coulen 20 20 ATING 20 20 N FACTOR 20 20 0 RATING 100.00 86.25 30.00 2	RBON VTING 100.00 86.25 30.00 23.00 0.100 0.075 20.05 20.05 1.00 0.025 20.010 20.01 20.01 1.00 0.0010 20.010 20.01 1.00 ATING 20.00 24.00 N FACTOR 20.00 24.00	RBOW VING 100.00 86.25 30.00 23.00 0.100 0.075 20.05 1.00 0.050 20 1.00 0.025 20 1.00 0.001 20 1.00 ATING 1.00 1.00 N FACTOR 1.00 24.00	RBON VTING 100.00 86.25 30.00 23.00 0.100 0.075 20.05 20.05 1.00 0.025 20.010 20.01 20.01 1.00 0.0010 20.010 20.01 1.00 ATING 20.00 24.00 N FACTOR 20.00 24.00	RBOW 1 TING 1 00 . 00 86 . 25 30 . 00 23 . 00 46 . 25 0 . 100 0 . 005 2 0 . 0 0 2 0 . 0 0 1 . 00 1 . 00 0 . 005 0 . 001 2 0 . 0 0 1 . 00 1 . 00 1 . 00 0 . 001 0 . 001 1 . 00 1 . 00 1 . 00 1 . 00 AATING A FACTOR 1 . 00 24 . 00 24 . 00 46 . 25	RBOW VING 100.00 86.25 30.00 23.00 0.100 0.075 20.05 1.00 0.050 20.050 1.00 0.025 20 1.00 0.001 20 1.00 COULER ATING 1.00 1.00 N FACTOR 1.00 24.00	Native 100.00 86.25 30.00 23.00 46.25 85.00	Nation N	Native 100.00 86.25 30.00 23.00 46.25 85.00 16.25 1.00 2.0	No.00 R6.25 30.00 23.00 46.25 R5.00 16.25 3.00 2.000	National 100.00 86.25 30.00 23.00 46.25 85.00 16.25 3.00 100.00

*WEIGHTED TOTAL DEPOSITS

CYLINDER LINER I.D. (IN) TEST #13

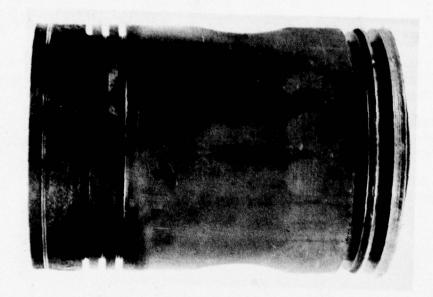
			Front/Back	k	Thr	ust/Antit	hrust
Су	linder	Par	allel to	Crank	Perpen	dicular to	o Crank
	No.	Top	Middle	Bottom	Top	Middle	Bottom
1.	After	3.8757	3.8760	3.8764	3.8769	3.8771	3.8767
	Before	3.8758	3.8761	3.8762	3.8762	3.8761	3.8763
	Change	-0.0001	-0.0001	0.0002	0.0007	0.0010	0.0004
2.	After	3.8759	3.8760	3.8767	3.8771	3.8768	3.8769
	Before	3.8757	3.8761	3.8734	3.8765	3.8765	3.8766
	Change	0.0002	-0.0001	0.0003	0.0006	0.0003	0.0003
3.	After	3.8760	3.8760	3.8763	3.8766	3.8771	3.8764
	Before	3.8760	3.8760	3.8762	3.8762	3.8761	3.8761
	Change	0.0000	0.0000	0.0001	0.0004	0.0010	0.0003
Ave	rage (All)	0.003					
	rage T/AT	0.006					

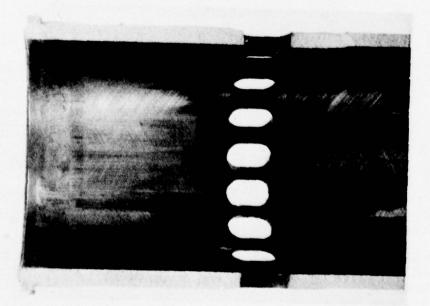
PISTON RING GAP (IN) TEST #13

					Ri	ng No.			
Pis	ston No.	1	2	3	4	5	6	7	8
1.	After	Stuck	0.032	0.026	0.036	0.026	0.026	0.026	0.026
	Before	0.031	0.031	0.026	0.035	0.023	0.023	0.023	0.023
	Change		0.001	0.000	0.001	0.003	0.003	0.003	0.003
2.	After	Stuck	0.033	0.033	0.035	0.025	0.025	0.025	0.025
	Before	0.34	0.033	0.033	0.034	0.022	0.022	0.022	0.023
	Change		0.000	0.000	0.001	0.003	0.003	0.003	0.002
3.	After	Stuck	0.029	0.027	0.027	0.025	0.025	0.026	0.026
	Before	0.031	0.029	0.027	0.027	0.023	0.022	0.023	0.023
	Change		0.000	0.000	0.000	0.002	0.003	0.003	0.003

Avg F/R (#1) Wear - All Stuck

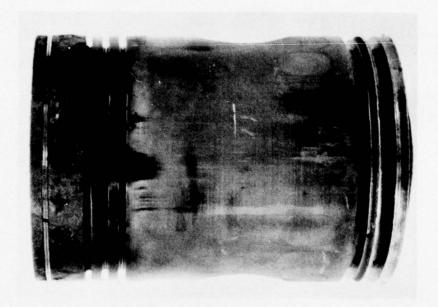
PISTON AND CYLINDER LINER CONDITION Test #13

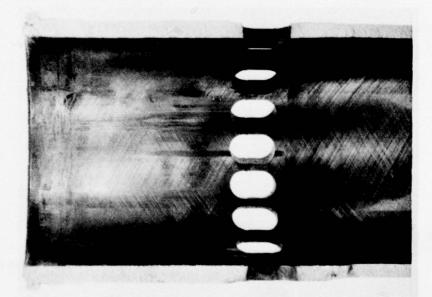




No. 2 - Antithrust Side (worst)

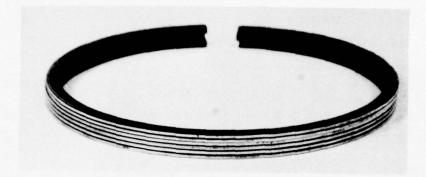
PISTON AND CYLINDER LINER CONDITION Test #13



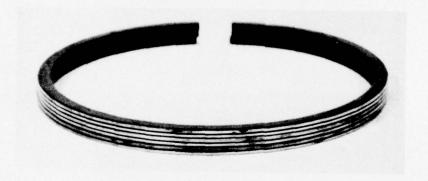


No. 2 - Thrust Side (best)

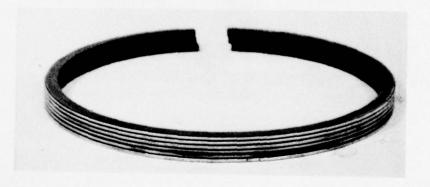
RING FACE CONDITION
Test #13



Piston - 1



Piston - 2



Piston - 3

APPENDIX G

3-53 TEST #14

FUEL: 1% S, DF-2

LUBE: AL-7287-L

START: 13 March 1978

END: 31 March 1978

ENGINE OPERATING DATA (AVG) TEST #14

	Min	Power Max	Avg	Idle (Avg)
Engine Speed, rpm Load, 1bs	2798 98	2809 104	2802 101	650
Torque, 1b-ft BHp obs	173 92	180 96	176 94	
Fuel Rate, 1b/hr BMEP, psi	38.3 81	43.3	40.4	
BSFC 1b/BHp-hr Temperatures, °F	0.417			
Jacket Coolant-In Jacket Coolant-Out	194 202	198 205	197 205	95 100
Oil Sump Inlet Air (Blower)	244 72	250	248	100
Exhaust Manifold Fuel @ Filter	910 72	990 95	947 89	
Pressures				
Oil Gallery, psig Blower Discharge, psig Intake Vacuum, in. H ₂ O Exhaust, Common, in. Hg	44 4.0 6.5 2.4	45 4.4 6.9 2.7	44 4.2 6.7 2.6	



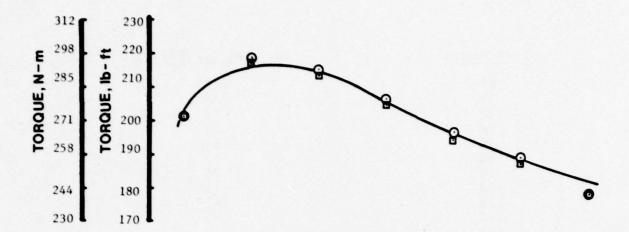
LUBRICANT ANALYSES AL-7287 TEST #14

Property	ASTM Method	New Oil	70 Hrs	140 Hrs	210 Hrs
K. Vis, cS, 40°C K. Vis, cS,100°C VI TAN	D445 D445 D2270 D664	103.3 11.4 96 2.2	126.6 13.1 96 3.6	134.0 13.7 97 3.9	136.6 13.9 98 4.4
TBN Insolubles, wt%	D2896 D893	13.7	12.8	13.2	12.3
Pentane A Benzene A					0.07
Pentane B Benzene B					0.08
Benzene B API Gravity, ° Pour Point, °C	D287 D97	25.5 -21			24.2
Flash Point, °C Carbon Residue, wt%	D92 D524	227 1.82	241 2.74	241 2.69	241 2.91
Sulfated Ash, wt% Elemental	D874 Method	1.63	1.96	2.08	2.13
Ba, ppm Mg, ppm	AA AA	< 50 20			
Ca, wt% Zn, wt%	AA AA	0.40	0.50 0.18	0.52 0.17	0.54 0.18
Na, ppm Cu, ppm	AA AA AA	6.20	5	6	6 5
Cr, ppm Pb, ppm Fe, ppm	AA AA XRF/AA		6 52/58	4 6 85/75	8 85/82
P, wt% S, wt%	XRF XRF	0.11 0.43			

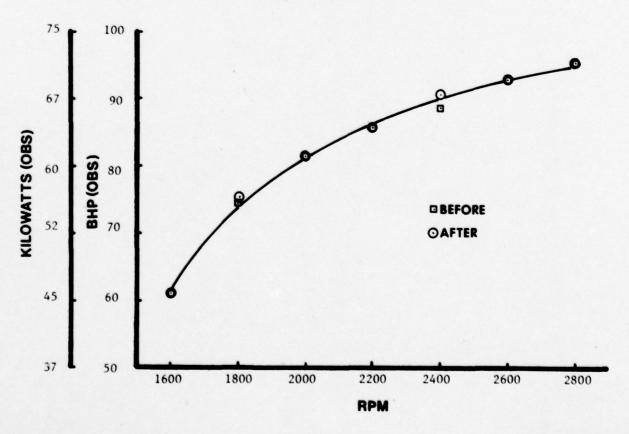
^{--- =} Not Determined.
AA = Atomic Absorption.
XRF = X-Ray Fluorescence.

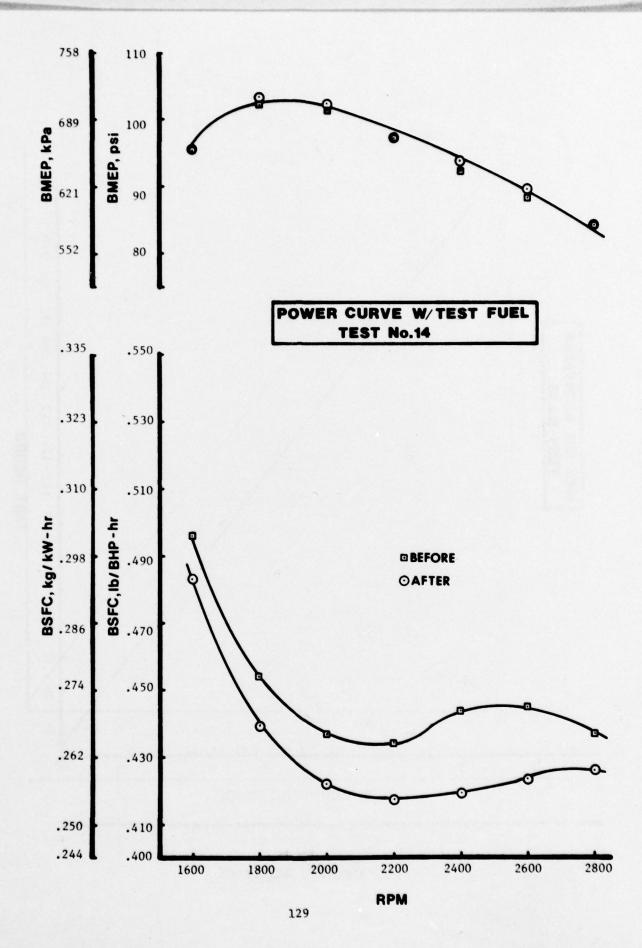
DAILY IRON CONTENT OF USED OIL TEST #14

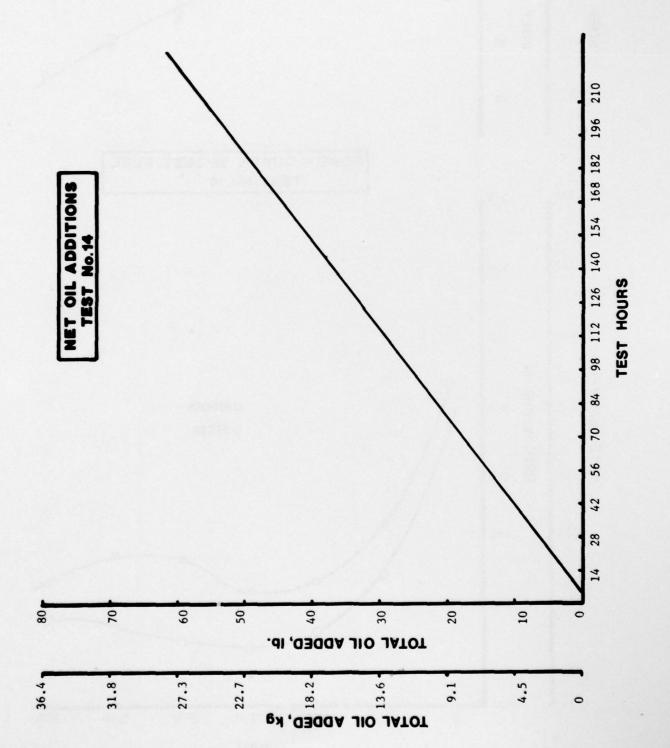
Test Hours	Fe, ppm (by KRF)
14	27
28	36
42	52
56	55
70	52
84	70
98	73
112	74
126	82
140	85
154	75
168	88
182	90
196	85
210	85



POWER CURVE W/ TEST FUEL TEST No.14







RING FACE CONDITION: % BURNING TEST #14

		Cylinder Number	
	1	2	3
First Ring	45	3	35
Second Ring	95	40	90
Third Ring	75	60	50
Fourth Ring	55	75	70
Average of all	58%		

N = Normal

RING STICKING TEST #14

Ring No.		Piston Number	
No.	1	2	3
1	F	30% cold stuck	F
2	F	.F	F
3	F	F	F
4	F	F	F

F = Free

CYLINDER LINERS TEST #14

% Lacquer 95 95 06 % Glazed 10 5 S Area Scuffed % Total Cylinder Liner Scuffing Percent of Compression Ring Travel Area 22 25 Anti-Thrust Percent Scuffed 40 35 35 Thrust 15 ∞ S S Percent Port Restriction Cylinder Number Average

PISTON O.D. (IN) TEST #14

3	3.8705	3.8705	0
2	3.8704	3.8704	0
	3.8707	3.8706	0.001
Cylinder	Before	After	

PISTON SURFACE CONDITION TEST #14

		Piston Number	
	1	2	3
Top Land	N	N	N
Skirt	Lt Scuff Lt Scratch	Lt Scratch	Lt Scratch
Piston Pin	N	N	N

N = Normal

PISTON GROOVE INSIDE DIAMETER - % RING SUPPORTING CARBON TEST #14

	•	P	iston Numb	er
Piston Ring	Quadrant	1	_2	3
	1	70	0	95
1	2	20	0	20
	3	0	5	85
	4	10	10	0
	1	15	0	10
2	2	20	30	90
	3	95	30	95
	4	100	0	15

Quadrants:

1 = Thrust

2 = Rear 3 = Anti-thrust 4 = Front

EXHAUST VALVE DEPOSITS TEST #14

	Cylinder No.
Area	1 2 3
Head	All AHC to soot except valve Cy #2=20% BHC
Face	All 8 & 9 lacquer
Tulip	All 1/2 AHC to AHC
Stem	All 1/2 AHC to soot & 9 lacquer

EXHAUST VALVE SURFACE CONDITIONS TEST #14

	Cylinder No.		
	1	2	3
Freeness in Guide	Free	Free	Free
Head	N	N	N
Face	Some pitting	N	N
Seat	N	N	N
Stem	N	N	N
Tip	N	N	N

N = normal

RING DEPOSITS TEST #14

CARB 2 LACQ	95-1/2AHC 5-6 0 80-7, 80-6 0 100-3 0 100-3	50-1/2HAC, 0	80-1/2AHC 0	90 1/2AHC 10-8 0 100-8	0 5-8,95-2	0 100-3 0 100-3 0 5-6, 95-c
LACQ	60-8, 20-6 95-1/ 100-8 100-5 100-3	20-8 50-1/	40-8 80-1/	0 100-8	10-6,20-4,	5-7, 05-3 5-6, 95-3 5-7, 95-3
CARB	20-1/2AHC 0 0 0	80-1/2AHC	60-1/2AHC	100-1/2AHC 0	0	000
Cylinder Number Piston	Top 1 2 3 3 4	1	2	х 4	Bottom 1	2 8 4

STANDARD COMPUTATION SHEET FOR PISTON RATING ATER LYONS DATE 4-6-78

LABORATORY TEST NUMBER 703-14 STAND NO. 2 ENGINE NO. 3D-131703 FUEL AL-7289-F RATER Lyons TEST HOURS 210 TEST LABORATORY AFLRL LUBRICANT AL-7287-L TEST PROCEDURE_

PISTON NO.

367
PISTON WTD. RATING

1					-			-							-				_	
_						GROOVES	VES							7	LANDS				INDER	ä
ō	TYPE	FACTOR	Z	NO. 1	S	NO. 2	NON NO	NO. 3	NO. 4	4	NO	-	N	NO. 2	NO.3	3	Ž	4.0%	CROWN	Z.
			AREA-%	AREA-% DEMERIT AREA-% DEMERIT	AREA-%			DEMERIT	AREA-%	DEMERIT	AREA.%	DEMERIT	AREA.%	DEMERIT	AREA-K	DEMERIT	AREA.%	AREAS DEMERIT AREAS DEMERIT AREAS DEMERITAREAS DEMERITAREAS DEMERIT AREAS DEMERITAREAS DEMERITAREAS DEMERIT	AREA.%	EWERIT
	HC	1.00	25	25.00	7.5	75.00			2	5.00	55	55.00	7.0	70.00						
	MHC	0.75					15	11.25												
NO	MC	0.50	S	2.50	2.5	6.25	ın	2.50							25	12.50				
887	27	0.25	70	17.50			80	20.00	55	13.75	40	10.00	15	3.75	40	10.00	15	3.75		
36	VLC	0.15							10	1.50	2	.75	10	1.50	15	2.25				
	25	CARBON	45.00	0	81.	.25	33.	75	19.2	25	65	.75	7.5	75.25	24.	7.5	3.	3.75		
	18	0.100											22	.50	2.0	2.00	25	2.50		
	DBrL	0.075															1		100	7 50
83	AL	0.050							30	1,50								1		
On	oni F	0.025																		
DA.	VAL	0.010																		
1_	RL	0.001																		
	7.6	LACQUER							1	.50			•	50	2	2.00	7.00	0.0	7.50	0
0	CLEAN	0																		
	ZONAL	ZONAL RATING																		
-	OCATION	LOCATION FACTOR																		
3	EIGHTE	WEIGHTED RATING	45.00	00	81.25	25	33.75	75	20.75	75	65.	75	75.	75	26.	26.75	10.7	75	7.50	0
														1						

*WEIGHTED TOTAL DEPOSITS

STANDARD COMPUTATION SHEET FOR PISTON RATING

TEST PROCEDURE 210 LABORAT TEST HOURS 210 STAND NG TEST LABORATORY AFLR STAND NG LUBRICANT AL-7287-L FUEL A

PISTON NO. 2	NO. 1 GROOVE, VOLUME %	PISTON WTD. RATING
ABORATORY TEST NUMBER 703-14	JEL AL-7289-F	

341

						GROOVES)VES							3	LANDS				3	UNDER.
0 1	DEPOSIT	DEPOSIT	ž	NO. 1	Z	NO. 2	ž	NO. 3	NO	NO. 4	NO.	-	S	NO. 2	Z	NO. 3	Ž	4.0N	CR	CROWN
			AREA-%	AREA-% DEMERIT AREA-% DEMERITA	AREA-%	DEMERIT		DEMERIT	AREA-%	DEMERIT	AREA-%	REA% DEMERIT AREA % DEMERITAREA % DEMERIT AREA % DEMERIT AREA % DEMERIT AREA % DEMERITAREA % DEMERIT	AREA-%	DEMERIT	AREA.%	DEMERIT	AREA.%	DEMERIT	AREA.%	DEMERI
	ž	8.1	10	10.00	55	55.00					65	65.00	75	75.00						
	MHC	0.75	20	37.50											4.6					
NO	WC.	0.50			45	22.50	40	20.00												
BRA	၁၂	0.25	35	8.75							10	2.50	10	2.50	4.5	11.25				
137	VLC	0.15	2	.75			10	1.50			20	3.00			40	6.00	2	.75		
	S.S.	CARBON	57	57.00	77	77.50	21	21.50			09	00.09	77	77.50	17	17.25		. 75		
	18	0.100					10	1.00	45	4.50	2	.50	15	1.50	5	.50	5	.50		
_	DBrL	0.075	-/												10	.75			100	7.50
8	AL	0.050					40	2.00	55	2.75										
סחו	LAL OUI	0.025															06	2.25		
AC	MA	0.010																		
1	RL	0.001		,																
	X7.	LACQUER					23	3.00	7.	7.25	5.50	50	1.50	50	1.	1.25	2.75	7.5	7	7.50
0	CLEAN	0																		
	ZONAL	ZONAL RATING																		
3	OCATION	LOCATION FACTOR																		
3	EIGHTEC	WEIGHTED RATING	57.00	00	77	77.50	24	24.50	7	7.25	99	00.99	79	79.00	18	18.50	3	3.50	7.50	50
				1								1								

STANDARD COMPUTATION SHEET FOR PISTON RATING

RATER Lyons DATE 4-6-78
LABORATORY TEST NUMBER 703-14
STAND NO. 2 ENGINE NO. 3D-131703
FUEL AL-7289-F

TEST PROCEDURE

TEST HOURS 210

TEST LABORATORY AFLRL

LUBRICANT AL-7287-E

PISTON NO. 3

NO. 1 GROOVE, VOLUME-%
PISTON WTD* RATING 401

_					GRC	GROOVES							\A	LANDS				DON	9
_	DEPOSIT	DEPOSIT	NO. 1	1.1	NO. 2		NO. 3	NO. 4	4	NO.	-	NO. 2	1	NO. 3	2	NO.	-	CROWN	N.
	34.	FACTOR	AREA-%	DEMERIT	AREA % DEMERIT	TAREA	* DEMERIT	AREA-% DI	EMERITA	IREA-% DI	EMERITA	AREA.%	EMERIT	AREA-%	EMERIT	AREA % DEMERIT AREA % DEMERIT	EMERIT	AREA.%	DEMERIT
<u> </u>	3	8.	09	60.00	75 75.0	00				80 8	80.00	9.0	90.00						
	MHC	0.75	10	7.50															
	S MC	0.50	30	15.00	25 12.5	0 35	17.50												
_	88 <i>k</i>	0.25						10 2	2.50	15	3.75	5	1.25	10	2.50	5	1.25		
38	O VLC	0.15								5	75	5	.75	15	2.25				
	3€	CARBON	82.50	0:	87.50	, ,	17.50	2.5	5.0	84.5	50	92	92.00	4.	4.75	1.25	25		
_	81	0.100												7.5	7.50	10 1	00.1		
	DBrL	0.075																100	7.50
	E AL	0.050				65	3.25	90 4	4.50							85 4	4.25		
	LAL LAL	0.025																	
	AC VE	0.010																	
<u> </u>	J.	0.001																	
	34	LACQUER					3.25	4.50	0.5					7.50	50	5.25	25	7.	7.50
	CLEAN	0																	
	ZONAL	ZONAL RATING																	
_	LOCATIO	LOCATION FACTOR																	
	WEIGHTE	WEIGHTED RATING	82.50	0	87.50	2(20.75	7.00	00	84.5	50	92.00	00	12.25	25	6.50	20	7.	7.50
' '	ייינולות	STISORSO IATOT OSTITOSSIII	020	DEITE															

CYLINDER LINER I.D. (IN)
TEST #14

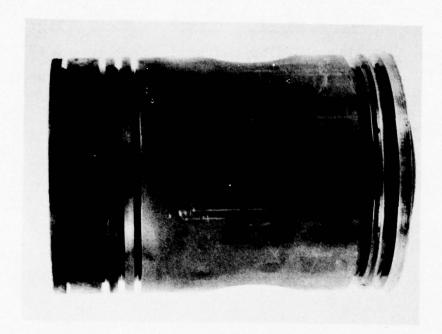
	linder No.		Front/Back llel to Cr Middle			st/Antithi dicular to <u>Middle</u>	
1.	Afte r Before Δ	3.8767 3.8762 0.0005	$\frac{3.8768}{3.8764}$ $\frac{0.0004}{0.0004}$	3.8772 3.8766 0.0006	$\begin{array}{r} 3.8771 \\ \underline{3.8762} \\ 0.0009 \end{array}$	$\frac{3.8774}{3.8764}$ $\frac{0.0010}{0.0010}$	3.8769 3.8764 0.0005
2.	After Before Δ	$\frac{3.8763}{3.8762}$ $\frac{0.0001}{0.0001}$	$\frac{3.8764}{3.8763}$ $\frac{0.0001}{0.0001}$	$\frac{3.8767}{3.8765}$ 0.0002	$\frac{3.8769}{3.8759}$ $\frac{0.0010}{0.0010}$	3.8769 3.8762 0.0007	3.8770 3.8764 0.0006
3.	After Before Δ	$\frac{3.8763}{3.8760}$ 0.0003	$\frac{3.8764}{3.8762}$ 0.0002	3.8767 3.8765 0.0002	3.8774 3.8764 0.0010	3.8776 3.8765 0.0011	3.8773 3.8766 0.0007

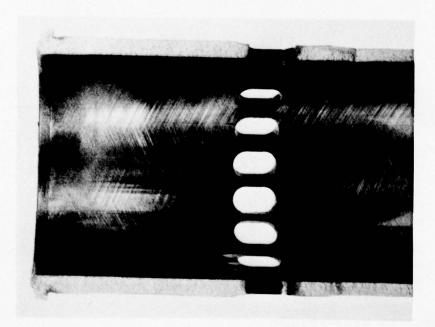
Average (A11) 0.0006 Average T/AT 0.0008

PISTON RING GAP (IN) TEST #14

					Ring	No.			
Pis	ton No.	<u> </u>	2	3	4	5	6		8
1.	After Before Δ	0.043 0.038 0.005	$0.031 \\ 0.031 \\ \hline 0.000$	$0.031 \\ 0.031 \\ \hline 0.000$	$0.032 \\ 0.031 \\ \hline 0.001$	$0.028 \\ 0.023 \\ \hline 0.005$	$ \begin{array}{r} 0.027 \\ 0.023 \\ \hline 0.004 \end{array} $	$ \begin{array}{r} 0.027 \\ 0.023 \\ \hline 0.004 \end{array} $	0.027 0.022 0.005
2.	After Before Δ	$0.036 \\ 0.033 \\ \hline 0.003$	0.035 0.035 0.000	$0.031 \\ 0.031 \\ 0.000$	$0.031 \\ 0.031 \\ 0.000$	0.027 0.022 0.005	0.027 0.023 0.004	0.027 0.022 0.005	0.027 0.023 0.004
3.	After Before A	0.041 0.036 0.005	$0.028 \\ 0.028 \\ \hline 0.000$	$0.031 \\ 0.031 \\ \hline 0.000$	0.023 0.023 0.000	0.025 0.021 0.004	0.025 0.022 0.003	$0.025 \\ 0.022 \\ \hline 0.003$	$0.025 \\ 0.022 \\ \hline 0.003$
Avg	F/R (#1) Wear	0.004						

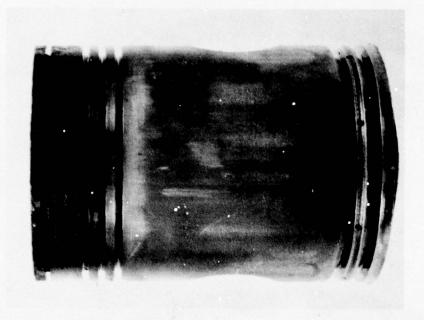
PISTON AND CYLINDER LINER CONDITION TEST #14

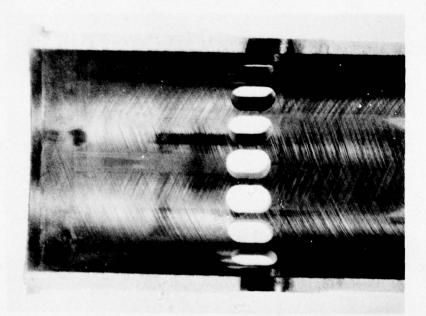




No. 2 - Anti-thrust Side (worst)

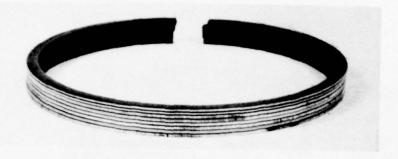
PISTON AND CYLINDER LINER CONDITION TEST #14



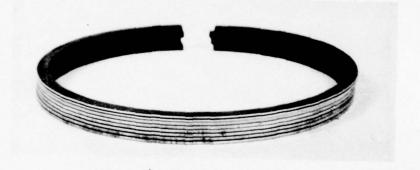


No. 3 - Thrust Side (Best)

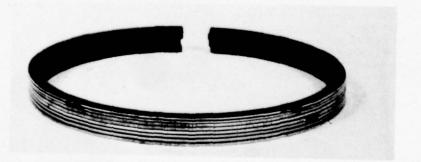
RING FACE CONDITION TEST #14



Piston - 1



Piston - 2



Piston - 3

APPENDIX H

3-53 TEST #16

FUEL: 1%S DF-2 (AL-7289-F)

LUBE: UK ER-5 (AL-6950-L)

START: 10 May 1978

END: 30 May 1978

ENGINE OPERATING DATA (AVG) TEST #16

	Min	Power	Avg	Idle (Avg)
				(AVB)
Engine Speed, rpm	2800	2806	2802	650
Load, 1bs	108	111	110	030
Torque, 1b-ft	189	194	192	
BHp obs	101	104	103	
Fuel Rate, 1b/hr	41.9	45.7	44.0	
BMEP, psi	90	92	91	
BSFC 1b/BHp-hr	0.408	0.449	0.430	
Temperatures, °F				
Jacket Coolant-In	196	198	197	95
Jacket Coolant-Out	203	205	205	100
Oil Sump	241	246	244	
Inlet Air (Blower)	78	99	89	
Exhaust Manifold	1000	1040	1017	
Fuel @ Filter	88	94	90	
Fuel Out	141	148	145	
Pressures				
Oil Gallery, psig	38	40	39	
Blower Discharge, psig	4.1	4.3	4.2	
Intake Vacuum, in. H ₂ 0	6.6	6.8	6.7	
Exhaust, Common, in. Hg	2.5	2.8	2.7	



LUBRICANT ANALYSES (AL-6950-L) TEST #16

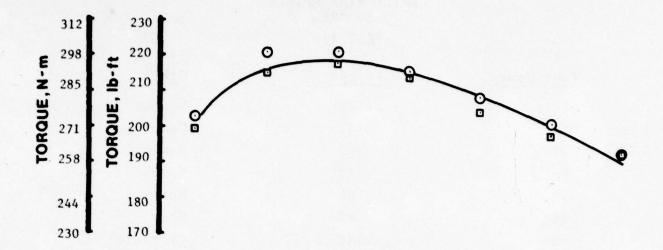
			1 1		
		New	70	140	210
Property	Method	011	Hrs	Hrs	Hrs
K. Vis, cS, 40°C	D445	59.67	56.00	58.85	60.09
K. Vis, cS, 100°C	D445	10.96	9.68	10.03	10.01
VI	D2270	178	158	158	153
TAN	D664	2.0	2.3	2.5	2.8
TBN	D2896	4.8	3.1	3.4	4.2
Insolubles, wt%	D893	1	7		
Pentane A	1	4	A	1	0.08
Benzene A					0.12
Pentane B				52	0.05
Benzene B	1				0.10
API Gravity, °	D287	29.1			27.1
Pour Point, °C	D97	-30		/2 //	
Flash Point, °C	D92	226	227	227	232
Carbon Residue, wt%	D524	0.56	1.36	1.64	1.74
Sulfated Ash, wt%	D874	0.73	0.85	0.95	1.00
Elemental	Method	10			
Ba, w%	AA	0.04			
Mg, ppm	AA	5			
Ca, wt%	AA	0.20	0.23	0.26	0.26
Zn, wt%	AA	0.09	0.11	0.11	0.11
Cu, ppm	AA		5	6	9
Cr, ppm	AA		5	9	11
Pb, ppm	AA		9	9	11
Fe, ppm	AA/XRF		61/80	103/136	114/149
S, wt%	XRF	0.92			

ND = Not Determined
AA = Atomic Absorption
XRF = X-Ray Fluorescence

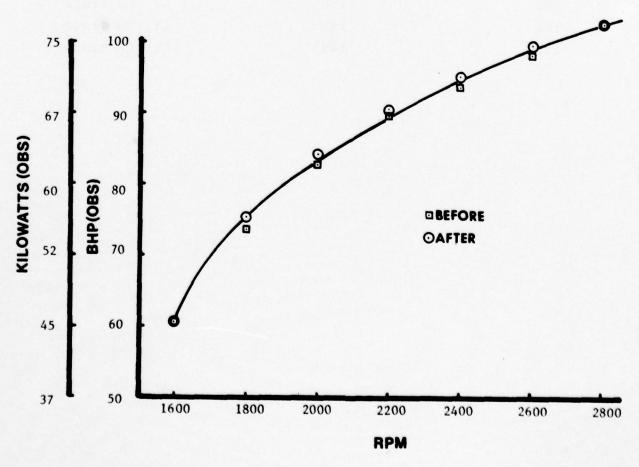
DAILY WEAR METALS BY XRF

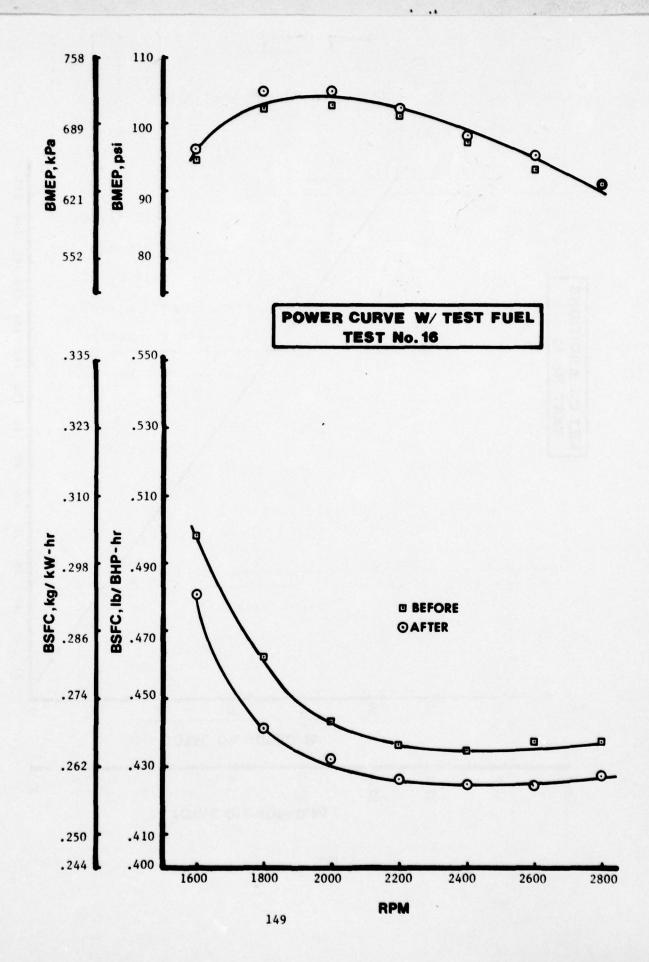
TEST #16

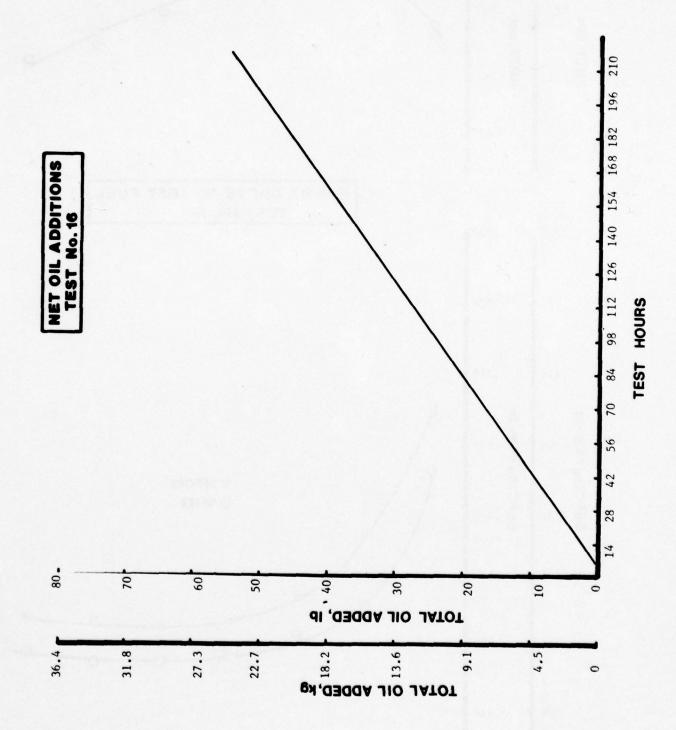
Test Hours	Fe ppm	Other
14	26	None
28	42	None
42	62	None
56	72	None
70	80	None
84	89	None
98	110	Cr trace
112	115	Cr trace
126	126	Cr, Cu trace
140	136	Cr, Cu trace
154	136	Cr, Cu trace
168	136	Cr, Cu trace
182	139	Cr, Cu trace
196	141	Cr, Cu trace
210	149	Cr, Cu trace



POWER CURVE W/ TEST FUEL TEST No.16







RING FACE CONDITION: % BURNING TEST #16

		Cylinder Number	r
	1	2	3
First Ring	2	10	35
Second Ring	5	70	95
Third Ring	25	50	80
Fourth Ring	10	35	90
Average of all	42%		

N = Normal

RING STICKING TEST #16

Ring No.	Pis	ton Number	
No.		2	3
1	10% cold stuck	F	F
2	F	F	F
3	F	F	F
4	F	F	F

F = Free

CYLINDER LINERS TEST #16

			ed % Lacquer	8 5	8.5	06	8.7
		,	% Glazed	15	15	10	13
Scuffing	ea	% Total	Area Scuffed	10	23	63	32
Cylinder Liner Scuffing	Travel Area	Percent Scuffed	Anti-Thrust	15	15	06	40
0 8		Perce	Thrust	S	30	35	23
		Percent Port	Restriction	ß	10	15	10
		Cylinder	Number	1	2	23	Average

PISTON O.D. (IN) TEST #16

$\frac{1}{2}$	3.8710 3.8705	3.8710	0 0
Cylinder	Before	After	V

PISTON SURFACE CONDITION TEST #16

		Piston Number	
		2	3
Top Land	N	N	N
Skirt	Lt scratches	Lt scratches V 1t scuff	Lt scratches V lt scuff
Piston Pin	N	N	N

N = Normal

PISTON GROOVE INSIDE DIAMETER - % RING SUPPORTING CARBON TEST #16

		P	iston Numbe	r
Piston Ring	Quadrant	1	2	3
	1	85	5	40
1	2	30	10	5
	3	100	0	0
	4	25	0	0
	1	0	100	20
2	2	85	20	25
	3	100	0	95
	4	0	25	40

Quadrants:

1 = Thrust

2 = Rear 3 = Anti-thrust

4 = Front

EXHAUST VALVE DEPOSITS TEST #16

		Cylinder No.	
Area	1	2	3
Head	ALL:	1/2 A to AHC	
Face	ALL:	100% #9 lacquer	
Tulip	ALL:	#9 lacquer to AHC	
Stem	ALL:	#9 lacquer to clean	

EXHAUST VALVE SURFACE CONDITIONS TEST #16

		Cylinder No.	
	_1	_2_	3
Freeness in Guide	F	F	F
Head	N	N	N
Face	N	N	N
Seat	N	N	N
Stem	N	N	N
Tip	N	N	N

F = Free N = Normal

RING DEPOSITS TEST #16

inder	Cylinder Number	CARB	1 LACQ	CARB 2	LACQ	CARB	3 LACQ
	1	25-AHC,15-1/2AHC	2AHC 60-8	100-AHC	0	30-1/2AHC	70-9
	2	0	100-8	0	100-8	0	90-8, 10-7
	3	0	75-8,25-3	0	100-3	0	100-4
	4	0	100-4	0	25-3,75-2	0	100-3
	1	100-AHC	0	100-AHC	0	100-AHC	0
	2	100-AHC	0	100-AHC	0	100-AHC	0
	3	100-1/2AHC	0	100-AHC	0	100-AHC	0
	4	0	100-8	100-1/2 AHC	0	0	100-9
Bottom	1	0	5-7, 95-3	0	20-6,25-7,55-3	0	50-5,45-4,5-8
	2	0	20-6, 80-2	0	100-2	0	100-2
	3	0	50-3, 50-2	0	190-2	0	50-4, 50-3
	4	0	85-3, 15-2	0	20-3, 80-2	0	100-3

STANDARD COMPUTATION SHEET FOR PISTON RATING

TEST LABORATORY
LUBRICANT AL-6950-L

TEST PROCEDURE_

PISTON NO.			NO. 1 GROOVE, VOLUME-%
RATER E R Lyons DATE 6-1-78	LABORATORY TEST NUMBER 703-16	STAND NO. 2 ENGINE NO.	FUELAL-7289-F

DEFO. DEFO																L	PISTO	NATO	PATIN	T	17.6
NO.1 NO.2 NO.3 NO.4 NO.5 NO.4 NO.5 NO.4 NO.5 NO.4 NO.4 NO.5 NO.4	L						000	93770							1					1	220
NO.1 NO.2 NO.3 NO.3 NO.4 NO.4 NO.4 NO.5 NO.3 NO.4 NO.5 NO.3 NO.4 CROWN NO.5							CHO	OVES							וב	SON				5	JER.
MAIL 1.000 60 60.00 50 50.00 15 15.00 15 15.00 10 10.00 40 40.00 30 30.00 40.00 10 10.00 10 10.00 10 10	7	POSIT	FACTOR	S.	-	Z	0.5	2	0.3	Z	4.0	N	1.1	Ň	2.5	ž	5.3	×	5.4	CRC	*
HC 1.00 60 60.0 50 15 15.0 15.0				AREA-%	DEMERIT	AREA-	KDEMERI		6 DEMERIT	AREA	% DEMERIT	AREA%	DEMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA.%	DEMERIT	AREAS	DEMERIT
MHC 0.75 12.50 15.50	-	S F	8.1		60.00		50.0	1	15.00			30	30.00		40.00		30.00				
Name		MHC																			
C 0.25 C 0.25	NO	1	0.50		20.00	2	12.5	1	7.50		5.00		7.			10	5.00			1	
VLC 0.15	88/		0.25			25	5.2			_		35	1	09	5.	2		4			
Record R	10																				
0.100 0.100 6.00 6.00 6.00 9 6.00 9 1.00 1.0		52	KRBON	80	00.0	67	.75	25.	0.0	5.	00	56.	. 25	55.	0.0	13	3.00	10	00.0		
0.056 CO.056 CO.056 </td <th></th> <th>BL</th> <th>0.100</th> <td></td> <td></td> <td></td> <td></td> <td>09</td> <td>6.00</td> <td>0</td> <td></td>		BL	0.100					09	6.00	0											
0.050 0.025 0.027 <th< td=""><th>_</th><th>DBrL</th><th></th><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>40</td><td>3.00</td><td></td><td>. 75</td><td></td><td> </td></th<>	_	DBrL														40	3.00		. 75		
0.025 0.026 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.025 0.0275 0.025 0.027	8	AL																			
0.001 COULD COULD 2.25 3.00 2.75 COUER NTING COULD 2.25 3.00 2.75 ODD APATING APATING <th>one</th> <th>LAL</th> <th></th> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>06</td> <td>. 2</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>40</td> <td>1.00</td> <td></td> <td></td>	one	LAL								06	. 2							40	1.00		
COULER COULER 6.00 2.25 3.00 2.75 ATING ATING 1 1 1 1 1 RATING A FACTOR 80.00 67.75 31.00 7.25 56.25 55.00 16.00 12.75	AC	VAL																			
80.00 6.00 2.25 3.00 2.75 80.00 67.75 31.00 7.25 56.25 55.00 16.00 12.75	1	RL																			
80.00 67.75 31.00 7.25 56.25 55.00 16.00 12.75		3,8	COUER					.9	0.0		.2					3.	0.0		5		
80.00 67.75 31.00 7.25 56.25 55.00 16.00 12.75	ರ	LEAN	0																		
80.00 67.75 31.00 7.25 56.25 55.00 16.00 12.75		ZONAL	RATING																		
80.00 67.75 31.00 7.25 56.25 55.00 16.00 12.75	3	CATION	W FACTOR																		
	3	EIGHTE	D RATING	80.	00	9	7.75	31	00.	7	.25	56.	2	55.	0.0	16.	00	12	1	10.	00

						ST/	NDA	STANDARD COMPUTATION SHEET FOR PISTON RATING	UTAT	ION SH	EET FO	OR PIST	TON RA	TING						
TES	TPRC	TEST PROCEDURE	E	1		RATER	8	E R Lyons	ons		DATE	6-1-78	78	١.	PIS	PISTON NO.	0.	2		
TES	TEST HOURS	URS	> 0			LABC	RATC	LABORATORY TEST NUMBER STAND NO 2 FINGINE NO	MUN T		703-1	9								
LE	LUBRICANT	LUBRICANT AL-6950	-6950	-		FUEL	AL-	FUEL_AL-7289-F							Z	0.1GR	OOVE,	NO. 1 GROOVE, VOLUME-%	E-%	
																PISTO	WTD.	PISTON WTD. RATING		461
						GROOVES	VES							LA	LANDS				3	SER.
DE	DEPOSIT	DEPOSIT	NO.	1.1	ž	NO. 2	ž	NO. 3	NO. 4	. 4	NO.	-	N	NO. 2	Š	NO.3	NO.	9.4	CRC	CROWN
			AREA-%	AREA-% DEMERIT AREA-% DEME	AREA-%		AREA-%	RITAREA% DEMERIT AREA% DEMERITAREA% DEMERITAREA% DEMERIT AREA% DEMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA.%	AREA.% DEMERIT AREA.% DEMER	AREA-%	DEMER
	5	1.00	09	60.00	09 0	60.00	10	10.00	20	20.00	20	20.00	09	60.00	5.0	50.00				
	MHC	0.75					20	15.00												
NO	S R	0.50	40	20.00	40	20.00	7.0	35.00	10	5.00							45	22.50		
887	2	0.25							5.5	13.75	40	10.00	2.5	6.50	35	8.75	15	3.75		
157	VLC	0.15									20	3.00								
	32	CARBON	80	80.00	80.00	0.0	60.00	0.0	38	38.75	33.00	0.0	99	66.25	58.7	7.5	26	26.25		
	86	0.100									20	2.00	1.5	1.50	15	1.50	10	1.00	100	10.0
_	DBrL	0.075																		
A	R AL	0.050							15	. 75										
סחו	LAL	0.025															30	.75		
DA.	WAL	0.010																		
1	RL	0.001					4													
	72	LACQUER							•	7.5	2	00.	1.	50	1.	50	1.75	5	10.00	0.0
Ö	CLEAN	0																		
	ZONAL	ZONAL RATING																		
3	CATIO	LOCATION FACTOR																		
3	SIGHTE	WEIGHTED RATING	80.00	0.0	80	80.00	9	00.09	39.50	50	35.00	0.0	67.75	7.5	60.25	25	28.00	0.0	10	10.00
3	EIGH	WEIGHTED TOTAL DEPOSITS	AL DEP	OSITS																

AREAS DEMENITAREAS DEMENITAREAS DEMENIT AREAS DEMENITAREAS DEMENITAREAS DEMENITAREAS DEMENITAREAS DEMENITAREAS 10.0 UNDER. CROWN 531 100 NO. 1 GROOVE, VOLUME % PISTON WTD . RATING 25.00 25.00 NO. 4 100 PISTON NO. 2.50 90.00 92.50 NO.3 10 10 10.00 90 90.00 90 LANDS 2.50 STANDARD COMPUTATION SHEET FOR PISTON RATING 92.50 NO. 2 90 22,50 10 LABORATORY TEST NUMBER 703-16 32.50 NO. 1 7.50 40 10.00 4.50 STAND NO. 2 ENGINE NO. FUEL AL-7289-F NO. 4 17.50 15 45 56.25 25.00 NO. 3 81.25 100 100.0 25 GROOVES 75 100.00 NO. 2 75.00 NO. 1 LUBRICANT AL-6950-L 75.00 100 TEST LABORATORY. *TEST PROCEDURE* FACTOR 0.100 0.010 0.075 0.050 0.025 DEPOSIT 8 0.75 0.50 0.25 0.15 CARBON TEST HOURS. TACOUER DBrL MHC VLC DEPOSIT S S 2 BL AL TYPE CARBON

WEIGHTED TOTAL DEPOSITS

10.00

25.00

92.50

92.50

32.50

22.00

81.25

100,00

75.00

WEIGHTED RATING

LOCATION FACTOR

ZONAL RATING

0

CLEAN

10.00

50

4

0.00

R

LACQUER

CYLINDER LINER I.D. (IN) TEST #16

	linder No.		Front/Back llel to Cr Middle			st/Antithi dicular to Middle	
1.	After Before A	3.8763 3.8760 0.0003	3.8765 3.8764 0.0001	3.8770 3.8766 0.0004	3.8772 3.8762 0.0010	3.8772 3.8763 0.0009	3.8771 3.8765 0.0006
2.	After Before A	3.8768 3.8760 0.0008	$\frac{3.8765}{3.8761}$ $\frac{0.0004}{0.0004}$	3.8768 3.8763 0.0005	$\frac{3.8775}{3.8761}$ $\frac{0.0014}{0.0014}$	$\frac{3.8774}{3.8763}$ $\frac{0.0011}{0.0011}$	$\frac{3.8771}{3.8765}$ $\frac{0.0006}{0.0006}$
3.	After Before Δ	3.8770 3.8761 0.0009	3.8766 3.8761 0.0005	3.8767 3.8763 9.0004	3.8775 3.8760 0.0015	3.8777 3.8762 0.0015	$\frac{3.8773}{3.8766}$ $\frac{0.0007}{0.0007}$

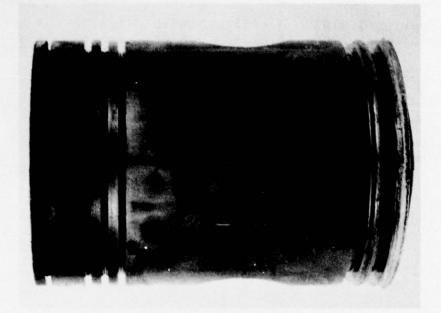
Average (A11) 0.0008 Average T/AT 0.0010

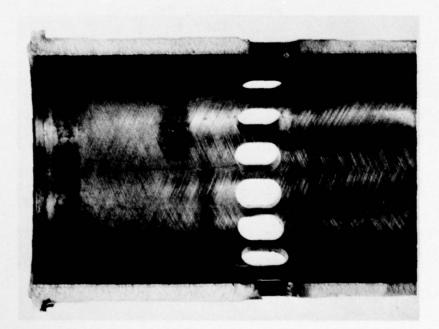
PISTON RING GAP (IN) TEST

					Ring	No.			
Pis	ston No.	1		3	4	5	6	7	8
1.	After Before Δ	$0.038 \\ 0.030 \\ \hline 0.008$	0.025 0.024 0.001	$\begin{array}{c} 0.022 \\ \underline{0.022} \\ 0 \end{array}$	0.046 0.044 0.002	$0.020 \\ 0.018 \\ \hline 0.002$	$0.020 \\ 0.018 \\ \hline 0.002$	0.022 0.019 0.003	0.023 0.020 0.003
2.	After Before Δ	$0.048 \\ 0.031 \\ 0.017$	$\begin{array}{c} 0.032 \\ \underline{0.032} \\ 0 \end{array}$	0.035 0.034 0.001	$0.031 \\ 0.030 \\ \hline 0.001$	$0.021 \\ 0.018 \\ \hline 0.003$	$0.020 \\ 0.018 \\ \hline 0.002$	0.021 0.018 0.003	$0.020 \\ 0.019 \\ 0.001$
3.	After Before Δ	$0.039 \\ 0.028 \\ \hline 0.011$	$\frac{0.027}{0.027}$	$\frac{0.034}{0.034}$	$0.023 \\ 0.023 \\ \hline 0$	$0.020 \\ 0.018 \\ \hline 0.002$	$0.022 \\ 0.018 \\ \hline 0.004$	0.021 0.018 0.003	$0.020 \\ 0.018 \\ 0.002$
				•					

Avg F/R (#1) Wear 0.012 in

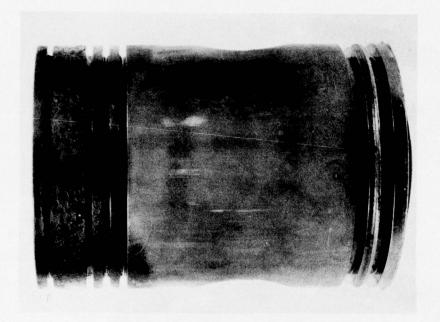
PISTON AND CYLINDER LINER CONDITION Test #16

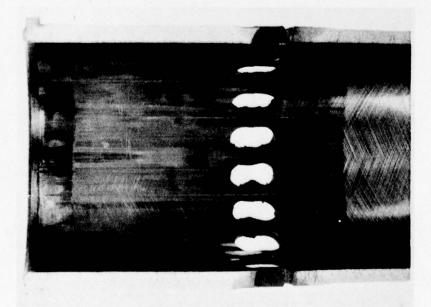




No. 1 - Thrust Side (best)

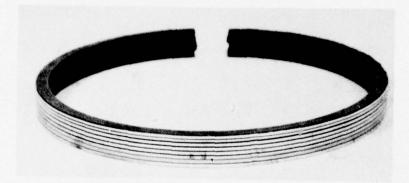
PISTON AND CYLINDER LINER CONDITION Test #16



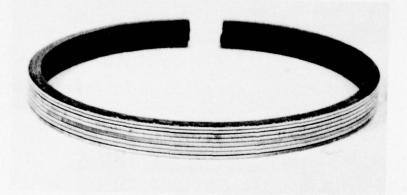


No. 3 - Antithrust Side (worst)

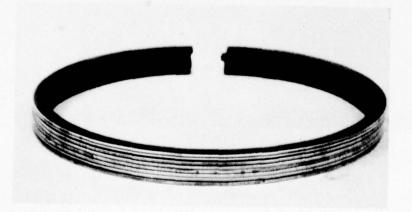
RING FACE CONDITION Test #16 . ..



Piston - 1



Piston - 2



Piston - 3

APPENDIX I

3-53 TEST #18

FUEL: High Sulfur Fuel (1%S), AL-7766

LUBE: REO 203

START: 11 Oct 78

END: 31 Oct 78

ENGINE OPERATING DATA (AVG) TEST #18

		Power		Idle
	Min	Max	Avg	(Avg)
Engine Speed, rpm	2800	2808	2802	651
Load, 1bs				
Torque, 1b-ft	177	196	190	
BHp obs	94	105	101	
Fuel Rate, 1b/hr	40.5	43.5	42.5	
BMEP, psi	84	93	90	
BSFC 1b/BHp-hr	0.408	0.444	0.420	
Temperatures, °F				
Jacket Coolant-In	196	198	197	96
Jacket Coolant-Out	205	205	205	100
Oil Sump	248	253	251	
Inlet Air (Blower)	70	90	82	
Exhaust Manifold	970	1030	1003	
Fuel @ Return	136	146	141	
Fuel @ Filter	85	94	90	
Pressures				
Oil Gallery, psig	42	43	43	
Blower Discharge, psig	4.2	4.5	4.4	
Intake Vacuum, in. H ₂ 0	6.8	6.9	6.8	
Crankcase, in. H ₂ 0 2	0.45	0.52	0.48	
Exhaust, Common, in. Hg	2.1	2.3	2.3	
Transfer Pump, psig	68	72	69	
Oil Consumption, 1b.			49.6	



LUBRICANT ANALYSES TEST #18

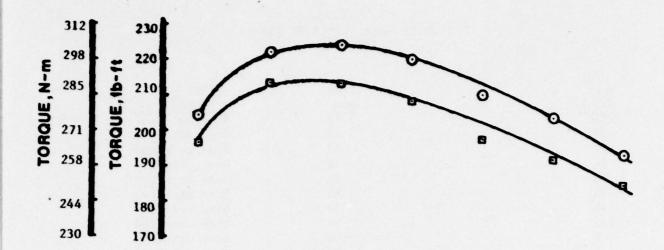
		New	70	140	210
Property	Method	011	Hrs	Hrs	Hrs
K. Vis, cS, 40°C	D445	104.6	112.3	118.7	121.0
K. Vis, cS, 100°C	D445	11.8	12.71	13.12	13.38
VI	D2270	101	106	105	106
TAN	D664	3.6	3.0	3.3	3.6
TBN	D2896	5.4	4.7	4.4	3.4
Insolubles, wt%	D893				
Pentane A		0.05	ND	ND	0.05
Benzene A		0.04	ND	ND	0.06
Pentane B		0.03	ND	ND	0.98
Benzene B		0.02	ND	ND	0.07
API Gravity, °	D287	27.5	ND	ND	26.5
Flash Point, °C	D92	241	. ND	ND	252
Carbon Residue, wt%	D524	1.19	1.79	1.98	2.15
Sulfated Ash, wt%	D874	0.93	ND	ND	1.25
<u>Elemental</u>	Method				
Ca, wt%	AA	0.24	0.29	0.30	0.31
Zn, wt%	AA	0.09	0.13	0.13	0.13
Cu, ppm	AA	ND	5	7	8
Cr, ppm	AA	ND	4	6	8
Pb, ppm	AA	ND	6	7	8
Fe, ppm	XRF/AA	ND	85/57	103/75	121/85

ND = Not Determined

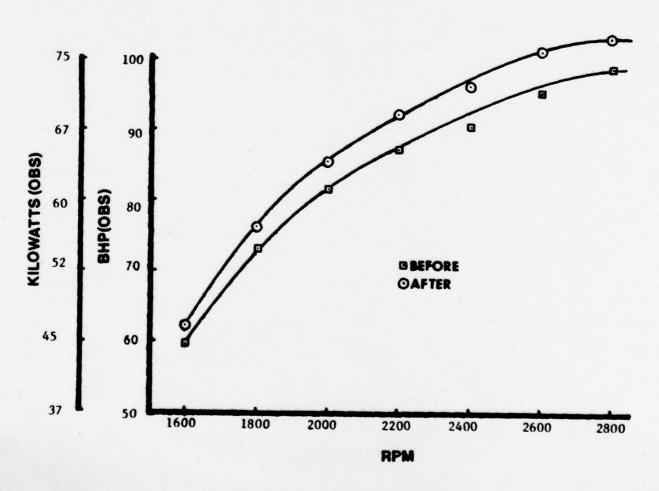
AA = Atomic Absorption XRF = X-Ray Fluorescence

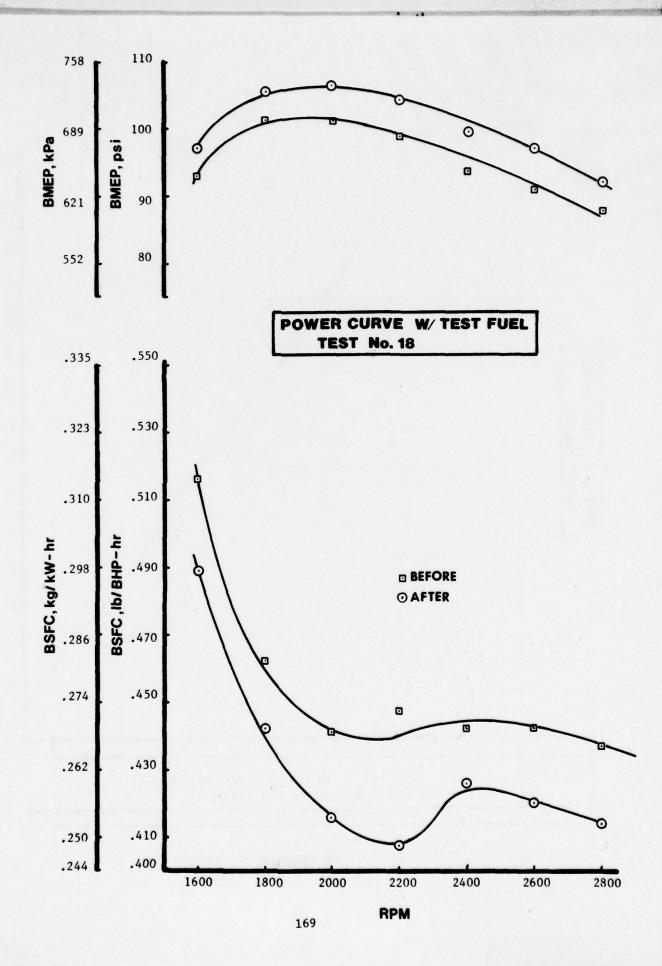
DAILY WEAR METALS BY XRF TEST #18

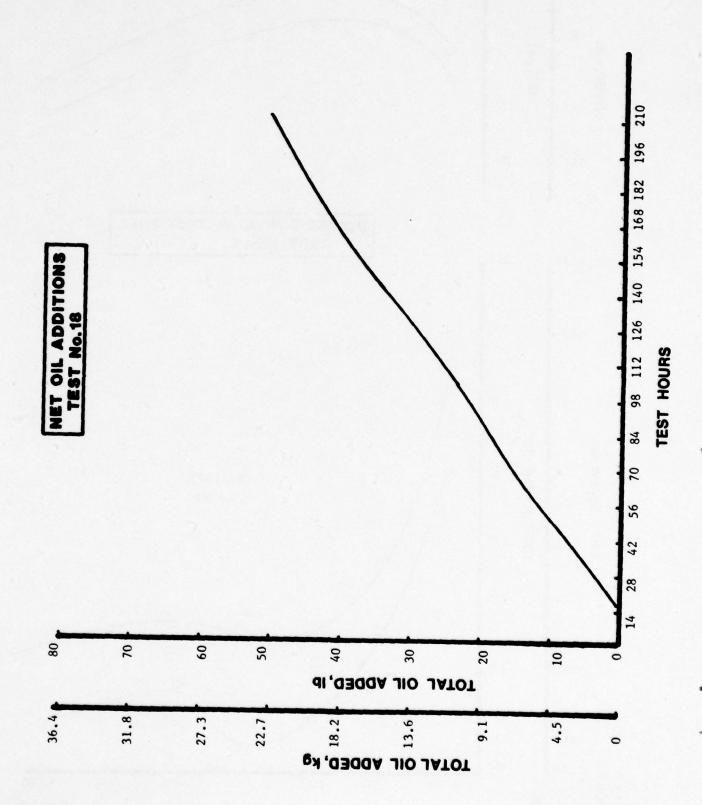
Test Hours	Iron ppm	Other Wear Elements
14	18	None detected
28	47	None detected
42	63	None detected
56	78	None detected
70	85	None detected
84	85	None detected
98	87	None detected
112	94	None detected
126	108	None detected
140	103	None detected
154	118	None detected
168	117	None detected
182	112	None detected
196	119	None detected
210	121	None detected



POWER CURVE W/ TEST FUEL TEST No.18







RING FACE CONDITION: % BURNING TEST #18

		Cylinder Number	
	1	2	3
First Ring	10	10	2
Second Ring	10	5	30
Third Ring	40	2	20
Fourth Ring	80	3	10
Average of all	19%		

N = Normal

RING STICKING TEST #18

Ring	Pis	ton Number	
Ring No.	1	2	3
1	F	F	F
2	F	F	F
3	5% Cold Stuck	F	F
4	F	F	F

F = Free

CYLINDER LINERS TEST #18

Cylinder Liner Scuffing Percent of Compression Ring Travel Area

D	Travel Area				
Percent Port Restriction			% Total		
	Thrust	Anti-Thrust	Area Scuffed	% Glazed	% Lacquer
2	10	75	43	5	95
2	85	40	63	15	85
2	20	30	25	10	90
2	38	48	44	10	90
	Restriction 2 2 2	Restriction Thrust 2 10 2 85 2 20	Restriction Percent Scuffed Thrust Anti-Thrust 2 10 75 2 85 40 2 20 30	Restriction Percent Scuffed Thrust Anti-Thrust Area Scuffed Area Scuffed % Total Area Scuffed 2 10 75 43 2 85 40 63 2 20 30 25	Percent Port Restriction Percent Scuffed Thrust Anti-Thrust Anti-Thrust Area Scuffed % Glazed 2 10 75 43 5 2 85 40 63 15 2 20 30 25 10 2 38 48 48 48

PISTON O.D. (IN) TEST #18

Cylinder	1	2	3
Before	3.8713	3.8705	3.8700
After	3.8711	3.8705	3.8700
Change	0.0002	0.0000	0.0000

PISTON SURFACE CONDITION TEST #18

		Piston Number	
	1	2	3
Top Land	Normal	Normal	Normal
Skirt	Sm Scratch A-T side	Normal	Normal
Piston Pin	Normal	Normal	Norma1

PISTON GROOVE INSIDE DIAMETER -% RING SUPPORTING CARBON TEST #18

		1	Piston Numbe	er
Piston Ring	Quadrant	1	2	3
1	1	0	0	0
	2	0	0	0
	3	0	0	0
	4	0	0	0
2	1	0	80	10
	2	95	0	30
	3	90	0	95
	4	0	40	5

Quadrants: 1 = Thrust

2 = Rear

3 = Anti-thrust

4 = Front

EXHAUST VALVE DEPOSITS TEST #18

	Cylinder No.				
Area Head	All Soot to 12 AHC				
Face	Very light pitting, all 100%-4 to lt. carbon				
Tulip	A11 100%-9 to ½ AHC				
Stem	All 100%-9 to clean				

EXHAUST VALVE SURFACE CONDITIONS TEST #18

		Cylinder No	
Freeness in Guide	<u>1</u>	<u>2</u>	<u>3</u>
Head	Normal	Normal	Normal
Face	Normal	Norma1	Normal
Seat	Normal	Normal	Normal
Stem	Normal	Normal	Normal
Tip	Normal	Normal	Normal

RING DEPOSITS TEST #18

11	1										
CARB	15-7	100-3	30-3	0	0	100-9	100-7	5-5	15-6	50-4	100-2
CARB 100-AHC	0	0	0	100-12AHC	100-13AHC	0	0	0	0	0	0
LACQ 0	30-8	100-7	100-2	0	00	0	100-9	20-5, 75-3	100-2	100-2	100-2
2 CARB 100-½ AHC	0	0	0	100-3анс	70-AHC 30-84 HC	25-AHC 75-5AHC	0	0	0	0	0
1ACQ 20-7	20-8	10-5	100-2	5-8	00	0	6-56	5-7, 90-2	5-7	100-3	100-2
CARB 60-½ AHC	0	0	0	95- ¹ 2AHC	75-AHC	100-12AHC	5-½AHC	0	0	0	0
Number Ring 1	2	3	7	1	2	8	4	-	2	3	4
Cylinder Number Ring Top				9				Bottom			

PISTON RING GROOVE DEPOSITS TEST # 18

	CARB	100-9	100-9	100-7	100-5	0	0	30-8	45-6	100-3	100-3	20-7	20-6 80-4
3	CARB	0	0	0	0	80-A 20-½AHC	35-B 65-AHC	45-AHC	0	0	0	80 -4, АНС	0
2	LACQ	100-8	25-8	60-8 40-6	30-7 70-4	0	0	0	100-9	30-7	45-8 55-5	50 - 7 50 - 5	100-3
	CARB	0	0	0	0	100 AHC	30-B 70 AHC	30-B 70% AHC	0	0	0	0	0
	1	6-06	100-4	100-4	100-4	0	0	0	80-7	100-4	100-5	100-5	100-4
	CARB	10-4 AHC	0	0	0	60-A 40-5AFC	30-B, 40-A 30-5AHC	100-AHC	20-AHC	0	0	0	0
Number	Ring		2	6	4	1	7	m	4	1	2	e .	4
Cylinder Number		of of	Groove			Back	Groove			Bottom	Groove		

STANDARD COMPUTATION SHEET FOR PISTON RATING DATE 11-7-78 703-18 LABORATORY TEST NUMBER—STAND NO. 2 ENGINE NO. 18S RATER Ed Lyons TEST LABORATORY AFLRI LUBRICANT AL-7219 TEST PROCEDURE 210

PISTON NO.

404 NO. 1 GROOVE, VOLUME-% PISTON WTD. RATING

_						GROO	OVES							LA	LANDS				No	UNDER.
_	DEPOSIT	DEPOSIT	NO.		ž	NO. 2	Z	NO. 3	NO. 4	4	NO.	-	N	NO. 2	Ž	NO.3	NO	7.4	S	CROWN
	1		AREA-%	AREA-% DEWERIT AREA-% DEMERI	AREA-X	DEMERIT	AREA-%	TAREAN DEMERIT AREAN DEMERIT AREAN DEMERITAREAN DEMERIT AREAN DEMERIT AREAN DEMERIT AREAN DEMERIT	AREA-%	DEMERI										
	¥	1.00	10	10.00	45	45.00					10	10.00	75	75.00						
	₹ HC	0.75	35	26.25			25	18.75	10	7.50					40	30.00				
.,,,	S NO	0.50	55	27.50	55	27.50	75	37.50	2	2.50	90	45.00	15	7.00						
1	2 LC	0.25													15	3.75				
.77	O VLC	0.15																		
	0.6	CARBON	,	63.75	72	72.50	56.	56.25	10.	10.00	55.00	0	82.	82.50	33.	33.75				
	BF.	0.100							85	8.50			10	1.00	45	4.50	35	3.50	100	10.00
-	DBrL	- 0.075															15	1.125		
	A AL	0.050															25	1.25		
	OU LAL	0.025															25	.625		
	SA ₹	0.010																		
•	J. R.	0.001																		
	3-	LACQUER							00	8.50			1.00	00	4	4.50	6.50)	10	10.00
	CLEAN	0																		
	ZONAL	ZONAL RATING																		
	LOCATIC	LOCATION FACTOR																		
	WEIGHT	WEIGHTED RATING	63.75	75	72	72.50	26	56.25	18.50	20	55.00	0(83.50	20	38.25	25	6.50	0	10.00	90
,	10.0	202 022	000	02.000																

111

10.00

19.125

27.25

88.00

31.25

11.50

62.50

76.25

55.00

WEIGHTED RATING LOCATION FACTOR ZONAL RATING

*WEIGHTED TOTAL DEPOSITS

10.00

3.25

43.00

92.50

47.50

7.00

30.00

85.00

75.00

WEIGHTED RATING

LOCATION FACTOR

ZONAL RATING

0

CLEAN

10.00

3.25

7.00

5.00

2.25

90

1.00

20

LACOUER AL O.025

0.00

R

LACQUER

CRC DIESEL RATING SYSTEM

STANDARD COMPUTATION SHEET FOR PISTON RATING

TEST LABORATORY AFLRE LUBRICANT AL-7219 TEST HOURS 210 TEST PROCEDURE_

DEPOSIT

DEPOSIT

FACTOR

TYPE

LABORATORY TEST NUMBER

STAND NO. 2 ENGINE NO. 703

FUEL AL-7666 RATER Ed Lyons

NO. 1 GROOVE, VOLUME-%

PISTON NO. _

	_		F	1	_	_	_			_	_		
393	UNDER.	CROWN	EAS DEMERIT AREAS DEMERIT AREAS DEMERITAREAS DEMERITAREAS DEMERIT AREAS DEMERITAREAS DEMERITAREAS DEMERIT							1.00 100 10.00			
	2	S	AREA-%							100			
RATIN		NO. 4	DEMERIT							1.00			
WTD.		Ž	AREA-%							10			
PISTON WTD. RATING		.3	DEMERIT			40.00		3.00	43.00				
	LANDS	NO. 3	AREA-%			80		20	43				
	4	.2	DEMERIT	go.06	,		2.50		20				
V		NO. 2	AREA-%				10		92.50				
		_	DEMERIT	30.00 90		10.00		7.50	47.50				
		NO.	AREA-%	30		20		50	47				
		NO. 4	9.4	0.4	0.4	DEMERIT							
			AREA-%								80		
		NO. 3	DEMERIT			25.00			00	5.00			
	VES	N	AREA-%			50			25.00	50			
	GROOV	. 2	DEMERIT	40.00	45.00				00				
		NO. 2	AREA-%	40					85.00				
		.1	REA-% DEMENITAREA-% DEMENITARE		75.00 60				00				
		NO. 1	AREA-%		100				75.00				

WEIGHTED TOTAL DEPOSITS

0.100 0.075 0.050

BE

DBrL

AL

CARBON

CARBON CARBON CARBON CARBON CARBON

0.75

MHC

8

¥

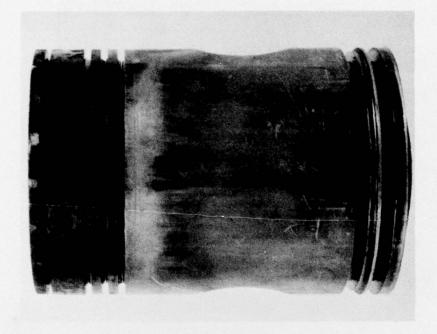
CYLINDER LINER I.D. (IN) TEST # 18

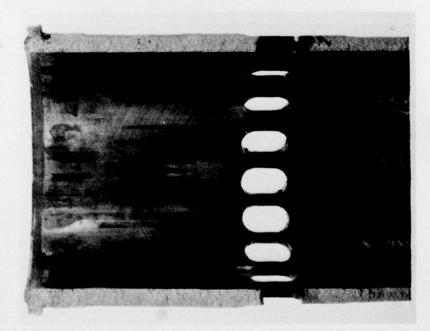
			Front/Back	k	Thr	ust/Antit	hrust
Су	linder	Para	allel to	Crank	Perpen	dicular to	o Crank
	No.	Тор	Middle	Bottom	Тор	Middle	Bottom
1.	After	3.8763	3.8766	3.8772	3.8774	3.8777	3.8775
	Before	3.8762	3.8765	3.8767	3.8761	3.8764	3.8767
	Change	0.0001	0.0001	0.0005	0.0013	0.0013	0.0008
2.	After	3.8766	3.8766	3.8766	3.8777	3.8777	3.8770
	Before	3.8766	3.8766	3.8766	3.8762	3.8763	3.8763
	Change	0.0000	0.0000	0.0000	0.0015	0.0014	0.0007
3.	After	3.8760	3.8760	3.8761	3.8770	3.8772	3.8766
	Before	3.8760	3.8760	3.8760	3.8759	3.8759	3.8759
	Change	0.0000	0.0000	0.0001	0.0011	0.0013	0.0007
Ave	rage (All)	0.0006					
	rage T/AT	0.0011					

PISTON RING GAP (IN) TEST # 18

					Rí	ng No.			
Pis	ton No.	1	2	3	4	5	6	7	8
1.	After	0.043	0.034	0.033	0.031	0.024	0.025	0.023	0.024
	Before	0.037	0.034	0.033	0.031	0.020	0.020	0.020	0.020
	Change	0.006	0.000	0.000	0.000	0.004	0.005	0.003	0.004
2.	After	0.054	0.035	0.033	0.032	0.020	0.020	0.019	0.023
	Before	0.032	0.034	0.032	0.031	0.018	0.017	0.017	0.019
	Change	0.022	0.001	0.001	0.001	0.002	0.003	0.002	0.004
3.	After	0.030	0.032	0.034	0.031	0.020	0.022	0.020	0.026
	Before	0.025	0.032	0.033	0.030	0.017	0.018	0.017	0.022
	Change	0.005	0.000	0.001	0.001	0.003	0.004	0.003	0.004
Avg	F/R (#1)	Wear	0.011						

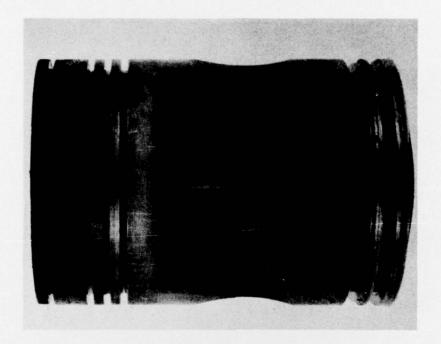
PISTON AND CYLINDER LINER CONDITION TEST NO. 18

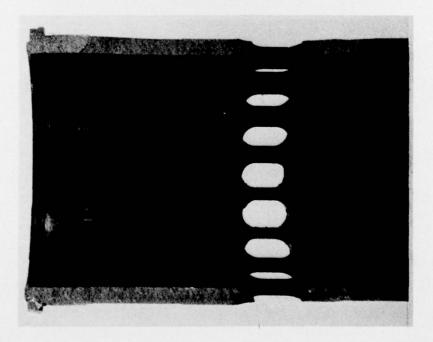




No. 2 - Thrust Side (Worst)

PISTON AND CYLINDER LINER CONDITION TEST NO. 18



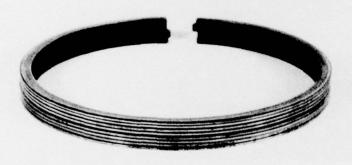


No. 1 - Thrust Side (Best)

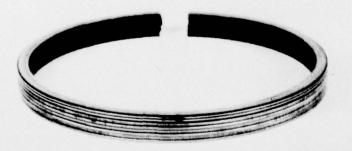
RING FACE CONDITION Test No. 18



Piston - 1



Piston - 2



Piston - 3

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DRSTS-MEG (2)	1	COMMANDER	
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		CORPUS CHRISTI TX 78419	

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CHEMICAL & BIOLOGICAL DIV		ABDEEN PVG GD MD 21005	
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COMMANDER		TONT KNOW KT 40121	
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STSGP-PE	1	ATTN STEYP-MTS	1
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		ATTN STEWS	1
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ATTN DRDTA-RT	1	WHITE SANDS NM 88002	
DRDTA-RC	1		
DRDTA-RG	2	COMMANDER	
DRDTA-J	1	ATTN OFC OF THE LIBRARIAN	
DRDTA-Z	1	US ARMY AVIATION SCHOOL	
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DRSTA-W	1	COMMANDER	
DRSTA-M	1	ATTN DRXMD-MS	1
DRSTA-GBP (MR MC CARTNEY)	1	DARCOM MRSA	
DRSTA-F	1	LEXINGTON KY 40507	
WARREN MI 48090			
		COMMANDER	
DIRECTOR		ATTN ATSM-CTD-MS (MAJ BREWSTER)	1
ATTN DRXSY-S	1	ATSM-CD-M	1
DRXSY-CM (MR WOOMERT)	1	ATSM-TNG-PT (LTC VOLPE)	1
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ATTN DRXST-MT1	1	ATSH-CD-MS-M	1
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COMMANDER		TTO NEW TORK 09310	
ATTN ATSAR-CTD-M	1	PROJ MGR M60 TANK DEVELOPMENT	
ATSB-TD	i	ATTN DRCPM-M60-TDT	1
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